

**Collective Torque Law**  $\vec{\tau}^{\text{EXT.}(A)} = d\vec{L}^{(A)} / dt$  [ derived in Lec 4B ]

For a collection of particles  $m_i$ , each with fixed mass, calculate the rate of change of total angular momentum relative to reference point A:

$$\frac{d\vec{L}^{(A)}}{dt} = \frac{d}{dt} \left( \sum_i \vec{r}_i^{(A)} \times m_i \dot{\vec{r}}_i^{(A)} \right) = \sum_i \dot{\vec{r}}_i^{(A)} \times m_i \dot{\vec{r}}_i^{(A)} + \sum_i \vec{r}_i^{(A)} \times m_i \ddot{\vec{r}}_i^{(A)}$$

The first term is zero  $\because$  the vector  $\dot{\vec{r}}_i^{(A)}$  is crossed with itself. In the second term, apply the defining relation  $\vec{r}_i^{(A)} \equiv \vec{r}_i - \vec{r}_A$  and the fact that  $m_i \ddot{\vec{r}}_i$  is the force on particle  $i$ :

$$\frac{d\vec{L}^{(A)}}{dt} = \sum_i \vec{r}_i^{(A)} \times m_i (\ddot{\vec{r}}_i - \ddot{\vec{r}}_A) = \sum_i \vec{r}_i^{(A)} \times \vec{f}_i - \sum_i \vec{r}_i^{(A)} \times m_i \ddot{\vec{r}}_A = \textcircled{1} - \textcircled{2}$$

Let's analyze these two sums  $\textcircled{1}$  and  $\textcircled{2}$  separately.

$$\textcircled{1} = \sum_i \vec{r}_i^{(A)} \times \vec{f}_i = \sum_i \vec{r}_i^{(A)} \times (\vec{f}_i^{\text{EXT}} + \vec{f}_i^{\text{INT}}).$$

$\vec{f}_i^{\text{INT}}$  is the total **internal** force on particle  $i$ , which is the sum of the forces exerted on it by every *other* particle  $j \neq i$  in the collection:

$$\begin{aligned} \textcircled{1} &= \sum_i \vec{r}_i^{(A)} \times \vec{f}_i^{\text{EXT}} + \sum_i \sum_{j \neq i} \vec{r}_i^{(A)} \times \vec{f}_{ij}^{\text{INT}} \\ &= \sum_i \vec{\tau}_i^{\text{EXT.}(A)} + \sum_i \sum_{j > i} \vec{r}_i^{(A)} \times (\vec{f}_{ij}^{\text{INT}} + \vec{f}_{ji}^{\text{INT}}) \end{aligned}$$

By **Newton's 3rd Law**, the forces between two particles are equal and opposite:  $\vec{f}_{ij} = -\vec{f}_{ji}$ , so the term in parentheses above is zero. Thus,

$$\textcircled{1} = \sum_i \vec{\tau}_i^{\text{EXT.}(A)} = \vec{\tau}^{\text{EXT.}(A)}$$

This is the total torque on the collection due to external forces. The relation we seek is  $d\vec{L}^{(A)} / dt = \vec{\tau}^{\text{EXT.}(A)}$ , and that is what we will get ... but only if sum  $\textcircled{2}$  is zero. Is it?

$$\textcircled{2} = \sum_i \vec{r}_i^{(A)} \times m_i \ddot{\vec{r}}_A = \left( \sum_i m_i \vec{r}_i^{(A)} \right) \times \ddot{\vec{r}}_A = M\vec{R}^{(A)} \times \ddot{\vec{r}}_A$$

This is zero under any of these conditions: if  $\vec{R}^{(A)} \equiv \vec{R} - \vec{r}_A = 0$ , if  $\ddot{\vec{r}}_A = 0$ , or if the cross-product is zero. Summarizing:

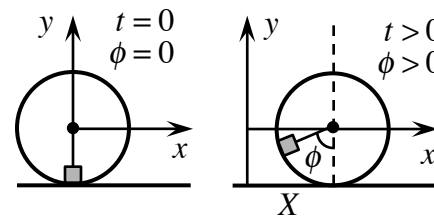
$\vec{\tau}^{\text{EXT.}(A)} = d\vec{L}^{(A)} / dt$  holds if

- A is not accelerating, or  $\rightarrow \ddot{\vec{r}}_A = 0$
- A is the CM, or  $\rightarrow \vec{R}^{(A)} = \vec{R}^{(CM)} = \vec{R} - \vec{r}_A = 0$
- $\ddot{\vec{r}}_A$  is parallel to  $\vec{R}^{(A)} \equiv \vec{R} - \vec{r}_A$   $\rightarrow \ddot{\vec{r}}_A \times \vec{R}^{(A)} = 0$

### Torque Law at the Contact Point of a Rolling Object

The third condition on the torque law,  $\ddot{\vec{r}}_A \parallel \vec{R}^{(A)}$ , does not apply to many problems. One important exception occurs for an object that is **rolling without slipping** along a surface. Let's call the rolling object a "wheel" for brevity. Let's also give it a radius  $b$  and have its CM move in the  $+x$  direction. The **instantaneous contact point** between the wheel and the surface is a valid reference point for the torque law, even though this point is accelerating and is not the CM.

Mentally paint a dot on the wheel's edge and call it point B. (In the figures below, it is indicated by a small grey square.) Point B is only in contact with the surface at a particular moment in time — that's why we call it an "instantaneous" contact point. Without loss of generality, we can choose our coordinates so that B is the contact point at time  $t = 0$  and CM position  $X = 0$ . We will also define the wheel's rotation angle  $\phi$  to be the angle that B makes with the downward vertical axis; contact then occurs at  $\phi = 0$ . This moment in time is shown in the left-hand figure. A later moment is shown on the right.



#### The no-slip rolling condition

between  $\phi$  and  $X$  is immediately clear from the right-hand figure: the arc length  $b\phi$  is exactly the horizontal distance travelled by the wheel, so  $X = b\phi$ . This condition is *essential* for the upcoming proof.

Our task is to show that the point B – the small square – satisfies the condition  $\ddot{\vec{r}}_B \parallel \vec{R}^{(B)}$  at the moment of contact, i.e. when  $t, \phi, X$  are all 0. At that moment (left-hand figure), the direction of  $\vec{R}^{(B)}$  = the vector pointing from B to the CM is upward, which is the  $+y$  direction.

We must now show that the acceleration  $\ddot{\vec{r}}_B$  of the point B is *also* in the y direction. In Cartesian coordinates, simple geometry gives us

$$\vec{r}_B(t) = \vec{R}(t) + \vec{r}'_B(t) = [X \hat{x}] + b[-\sin\phi \hat{x} - \cos\phi \hat{y}].$$

Note:  $X$  and  $\phi$  can be arbitrarily complicated functions of time. For example, the surface on which the wheel is rolling may be tilted, causing the wheel to accelerate under gravity. Any manner of external forces may be at work; the only restriction we are imposing on  $X$  and  $\phi$  is the no-slip rolling condition  $\dot{X} = b\dot{\phi}$  that ties them together.

We now calculate the acceleration of the point B:

$$\dot{\vec{r}}_B(t) = [\dot{X} \hat{x}] + b[-\dot{\phi} \cos\phi \hat{x} + \dot{\phi} \sin\phi \hat{y}]$$

$$\ddot{\vec{r}}_B(t) = [\ddot{X} \hat{x}] + b[(-\ddot{\phi} \cos\phi + \dot{\phi}^2 \sin\phi) \hat{x} + (\ddot{\phi} \sin\phi + \dot{\phi}^2 \cos\phi) \hat{y}]$$

We only need this acceleration at the moment when B *is* the contact point, i.e. when  $t = 0$  and  $\phi = 0$ . Since  $\cos(0) = 1$  and  $\sin(0) = 0$ ,

$$\ddot{\vec{r}}_B|_{t=0} = [\ddot{X} \hat{x}] + b[-\ddot{\phi} \hat{x} + \dot{\phi}^2 \hat{y}] = (\ddot{X} - b\ddot{\phi}) \hat{x} + b\dot{\phi}^2 \hat{y}$$

This acceleration is indeed in the y direction, just like  $\vec{R}^{(B)}$ , because the no-slip rolling condition kills the x-component :

$$X = b\phi \rightarrow (\ddot{X} - b\ddot{\phi}) = 0 \rightarrow \ddot{\vec{r}}_B|_{t=0} = b\dot{\phi}^2 \hat{y}$$

We have thus proved that the **contact point B** on a wheel that is **rolling without slipping** is a valid reference point for the torque law,  $\vec{\tau}^{(B)} = \dot{\vec{L}}^{(B)}$ , even though B *is* accelerating and is *not* the CM.

**Remarks** : This is an extremely useful result for two reasons.

- (1) The contact point is located on the wheel so it is **body-fixed**. That means we can use  $\vec{L}^{(B)} = I^{(B)}\omega \rightarrow$  no need to invoke the spin-orbit decomposition  $\vec{L}^{(A)} = \vec{L}_{CM}^{(A)} + \vec{L}'$  that we would need for a reference point located *outside* the wheel.
- (2) The torque  $\tau^{(B)}$  around the contact point does **not** depend on the **force of friction**, which is always present in no-slip rolling and is never known in advance.

## Collective Kinetic Energy – Rotational

An extended object can be both moving and rotating. Let's first calculate its total kinetic energy due **only** to its **rotation**, relative to any **body-fixed point B**. (The object cannot move *relative to itself*, so a body-fixed reference point isolates the rotational motion.)

$$\begin{aligned} T_{\text{rotational}}^{(B)} &= \frac{1}{2} \sum_i m_i |\dot{\vec{r}}_i^{(B)}|^2 = \frac{1}{2} \sum_i m_i |\vec{\omega} \times \vec{r}_i^{(B)}|^2 = \frac{1}{2} \sum_i m_i (\omega r_{i\perp}^{(B)})^2 \\ &= \frac{1}{2} \omega^2 \sum_i m_i (r_{i\perp}^{(B)})^2 = \boxed{\frac{1}{2} I^{(B)} \omega^2 = T_{\text{rotational}}^{(B)}} \end{aligned}$$

## Collective Kinetic Energy – Decomposition

To obtain a kinetic energy formula that includes both the rotational and linear motion of an extended object, let's introduce a **reference point A** other than the origin. Our aim is to find a good choice for A that will split the total KE into two terms: one for rotational motion and one for linear motion.

$$\begin{aligned} T &= \frac{1}{2} \sum_i m_i (\dot{\vec{r}}_i \cdot \dot{\vec{r}}_i) = \frac{1}{2} \sum_i m_i (\dot{\vec{r}}_i^{(A)} + \dot{\vec{r}}_A) \cdot (\dot{\vec{r}}_i^{(A)} + \dot{\vec{r}}_A) \\ &= \frac{1}{2} \sum_i m_i (\dot{\vec{r}}_i^{(A)} \cdot \dot{\vec{r}}_i^{(A)} + 2\dot{\vec{r}}_A \cdot \dot{\vec{r}}_i^{(A)} + \dot{\vec{r}}_A \cdot \dot{\vec{r}}_A) \\ &= \frac{1}{2} \sum_i m_i v_i^{(A)2} + \vec{v}_A \cdot \sum_i m_i \dot{\vec{r}}_i^{(A)} + \frac{1}{2} v_A^2 \sum_i m_i \\ &= T^{(A)} + \vec{v}_A \cdot \vec{V}_{CM}^{(A)} + \frac{1}{2} M v_A^2 \end{aligned}$$

To reduce this to two terms, we can do one of two things:

- (1) Choose A to be the CM : This kills the middle term, since  $V_{CM}^{(A)}$  becomes "velocity of the CM relative to the CM", which is zero. The right-hand term becomes  $\frac{1}{2} M v_{CM}^2 = \frac{1}{2} M V^2 = T_{CM}$ . Thus, 
$$\boxed{T = T_{CM} + T'} = \frac{1}{2} M V^2 + \frac{1}{2} I' \omega^2$$
. That's linear KE + rotational KE, just as we wanted, but this lovely split **only** occurs with A = CM.
- (2) Choose A to be a stationary point : If  $v_A = 0$ , we simply get 
$$\boxed{T = T^{(A \text{ stationary})}} \rightarrow T$$
 relative to the origin is the same as  $T$  relative to any other point that isn't moving (which is fairly obvious).