# Phys 326 Discussion 15 – Stress and Strain in a Solid

The stress tensor  $\Sigma$  (or  $\sigma_{ij}$  when index notation is in use) describes the <u>surface forces per unit area</u> on a differential element of area  $d\vec{A}$  within a material.  $d\vec{A}$  always points <u>outward</u> from the element experiencing the force. All this is summarized by the somewhat wordy equation

$$\vec{F}_{\text{acting on}}^{\text{surface}} = \Sigma \ d\vec{A}_{\text{OUT}} \qquad \dots \text{ or in index notation: } F_i^{\text{surface}} = \sigma_{ij} dA_j$$

The strain tensor **E** (or  $\varepsilon_{ij}$  in index notation) describes the <u>fractional deformation</u> of a material under stress. When stress is applied to a tiny element of material at location  $\vec{r}$ , it moves from its original position  $\vec{r}$  to a slightly shifted position  $\vec{r}' = \vec{r} + \vec{u}(\vec{r},t)$ . The function  $\vec{u}(\vec{r},t)$  is called the **displacement field** of the material.

<u>no strain</u>: element at  $\vec{r} \rightarrow$  <u>under strain</u>: element moves to  $\vec{r}' = \vec{r} + \vec{u}(\vec{r},t)$ 

We assuming all displacements are small (as they generally are in a solid). The strain tensor is directly related to the displacement field : it is a symmetrized version of the **derivative matrix D** :

$$\mathbf{D}_{ij} \equiv \frac{\partial u_i}{\partial r_j} = \begin{pmatrix} \partial_x u_x & \partial_y u_x & \partial_z u_x \\ \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots \end{pmatrix} \longrightarrow \mathbf{E} \equiv \frac{\mathbf{D} + \mathbf{D}^T}{2} = \begin{pmatrix} \partial_x u_x & \frac{1}{2} (\partial_y u_x + \partial_x u_y) & \vdots \\ \frac{1}{2} (\partial_x u_y + \partial_y u_x) & \partial_y u_y & \vdots \\ \vdots & \vdots & \vdots & \vdots \end{pmatrix}$$

(Here I'm using the familiar shorthand  $\partial_j u_i \equiv \partial u_i / \partial r_j$ .) As we learned, "stress / strain = elastic modulus", for various types of stress, strain and modulus (BM=Bulk, YM=Young's, SM=Shear Modulus). The formal relation between the stress and strain tensors is the **generalized Hooke's Law**. Here it is in " $F = k\Delta x$ " and " $\Delta x = F/k$ " forms, where I am making an analogy between the familiar  $F, k, \Delta x$  for a spring and our new  $\Sigma$ , M, E quantities.

• 
$$\Sigma = (\alpha - \beta)e \mathbf{1} + \beta \mathbf{E}$$
  
•  $\mathbf{E} = \frac{1}{3\alpha\beta} \Big[ 3\alpha \ \Sigma - (\alpha - \beta)(\operatorname{tr} \Sigma) \mathbf{1} \Big]$  where  $\alpha = 3BM$   
where  $\beta = 2SM$  and  $YM = \frac{3\alpha\beta}{2\alpha + \beta} = \frac{9BM \cdot SM}{3BM + SM}$   
 $e = \frac{1}{3}\operatorname{tr} \mathbf{E}$ 

#### **Problem 1 : An Example Stress Tensor**

It is found that the stress tensor in a continuous medium has the form given at right : (Ignore the units  $\odot$ .) Find the surface force  $\vec{F}^{\text{surf}}$  on a small area *dA* of the surface  $x^2 + y^2 + 2z^2 = 4$  at the point (x, y, z) = (1, 1, 1).

### **Problem 2 : Longitudinal Waves on a String**

A taut, massive string can support longitudinal waves as well as transverse ones. Suppose we have a string of cross-sectional area A, made of a material with Young's Modulus YM, and lying along the x axis. The displacement field for this string is  $\vec{u}(\vec{r},t) = u_x(x,t)\hat{x}$  since this problem is entirely 1-dimensional.

(a) Consider a very short piece of string of length *l*. We defined Young's Modulus as follows:

<sup>1</sup> 
$$\vec{F} = dA(2\hat{x} - \hat{y} - \hat{z}) / \sqrt{6}$$
  
<sup>2</sup> (b)  $\frac{\partial^2 u_x}{\partial t^2} = \frac{YM}{\rho} \frac{\partial^2 u_x}{\partial x^2}$  (c)  $c = \sqrt{YM / \rho}$ 

Checkpoints 1

$$= \left( \begin{array}{ccc} xz & z^2 & 0 \\ z^2 & 0 & -y \\ 0 & -y & 0 \end{array} \right)$$

$$YM = \frac{\text{tension-stress}}{\text{tension-strain}}$$
 where  $\text{tension-stress} = \frac{T}{A_{\perp}}$  and  $\text{tension-strain} = \frac{\Delta l}{l}$ 

Using <u>primes</u> to denote conditions under strain, as in  $\vec{r} \rightarrow \vec{r}' = \vec{r} + \vec{u}(\vec{r},t)$ , the tension-strain can be written  $\Delta l/l = (l'-l)/l$ . Considering what happens to the ends of the string under strain, show that the tension is related to Young's Modulus by  $T = A(YM)\partial u/\partial x$ .

(b) Now consider the <u>forces</u> on the ends of the little piece of string. Using F = ma, find the equation of motion for the longitudinal disturbance  $u_x(x,t)$ . Hint: to help you find the differential equation you seek, change notation a bit  $\rightarrow$  change the string segment's length from *l* to *dx* and put its center at some position *x*.

(c) What is the speed of longitudinal wave propagation along this string?

## **Problem 3 : Young's Modulus Relation**

## Checkpoints <sup>3</sup>

We didn't impose any conditions on the cross-sectional area A of the string in problem 2 so the string can be a solid block. Suppose the tension in the block of material in the x-direction only (as for the string) and constant :  $\vec{T}(\vec{r}) = T \hat{x}$ .

(a) Write down the stress tensor  $\Sigma = \sigma_{ij}$  for this block under constant tension. Then use the " $\Delta x = F/k$ " form of generalized Hooke's Law (the second bullet on the previous page) to write down the strain tensor  $\mathbf{E} = \varepsilon_{ij}$  in terms of the material constants  $\alpha$  and  $\beta$  and the <u>one</u> non-zero stress-tensor element  $\sigma_{ij}$  you obtained.

(b) Using the tension-stress & tension-strain analysis you already performed in problem 2, convince yourself that Young's Modulus is YM = one-element-of- $\sigma$  / one-element-of- $\varepsilon$ . (which elements?)

(c) Combine these results to derive the expression on the previous page for YM in terms of  $\alpha$  and  $\beta$ .

<sup>3</sup> (a) 
$$\mathbf{E} = \frac{\sigma_{11}}{3\alpha\beta} \begin{pmatrix} 2\alpha + \beta & 0 & 0 \\ 0 & \beta - \alpha & 0 \\ 0 & 0 & \beta - \alpha \end{pmatrix}$$
 (b)  $\mathbf{Y}\mathbf{M} = \frac{\sigma_{11}}{\varepsilon_{11}}$