

ECE 330

POWER CIRCUITS AND ELECTROMECHANICS

LECTURE 12

ELECTROMECHANICAL SYSTEMS (2)

Acknowledgment-These handouts and lecture notes given in class are based on material from Prof. Peter Sauer's ECE 330 lecture notes. Some slides are taken from Ali Bazi's presentations

Disclaimer- These handouts only provide highlights and should not be used to replace the course textbook.

ROTATIONAL SYSTEM

This is the basic configuration of many machines.

Both rotor and stator have $\mu = \infty$.

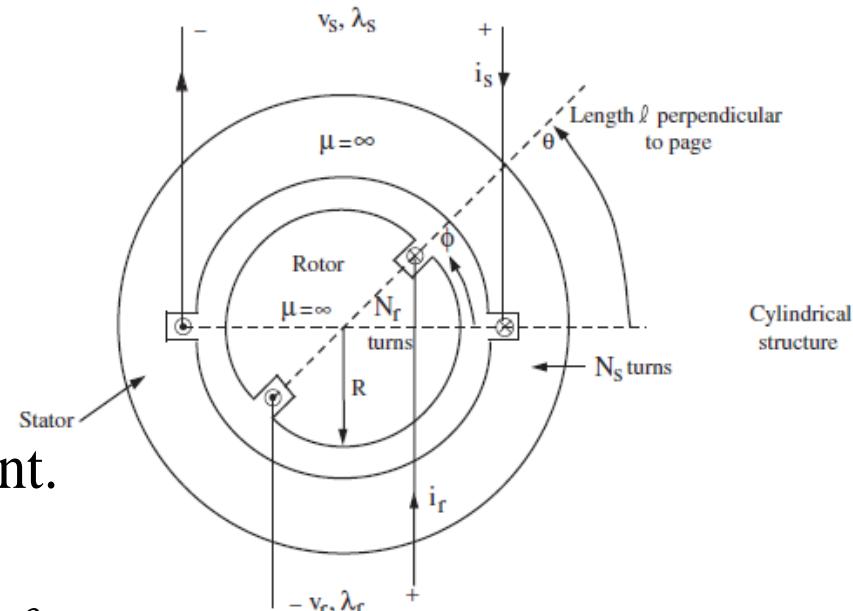
The radial air gap has length g .

The cylindrical rotor is of length ℓ .

At time t , θ is the angular displacement.

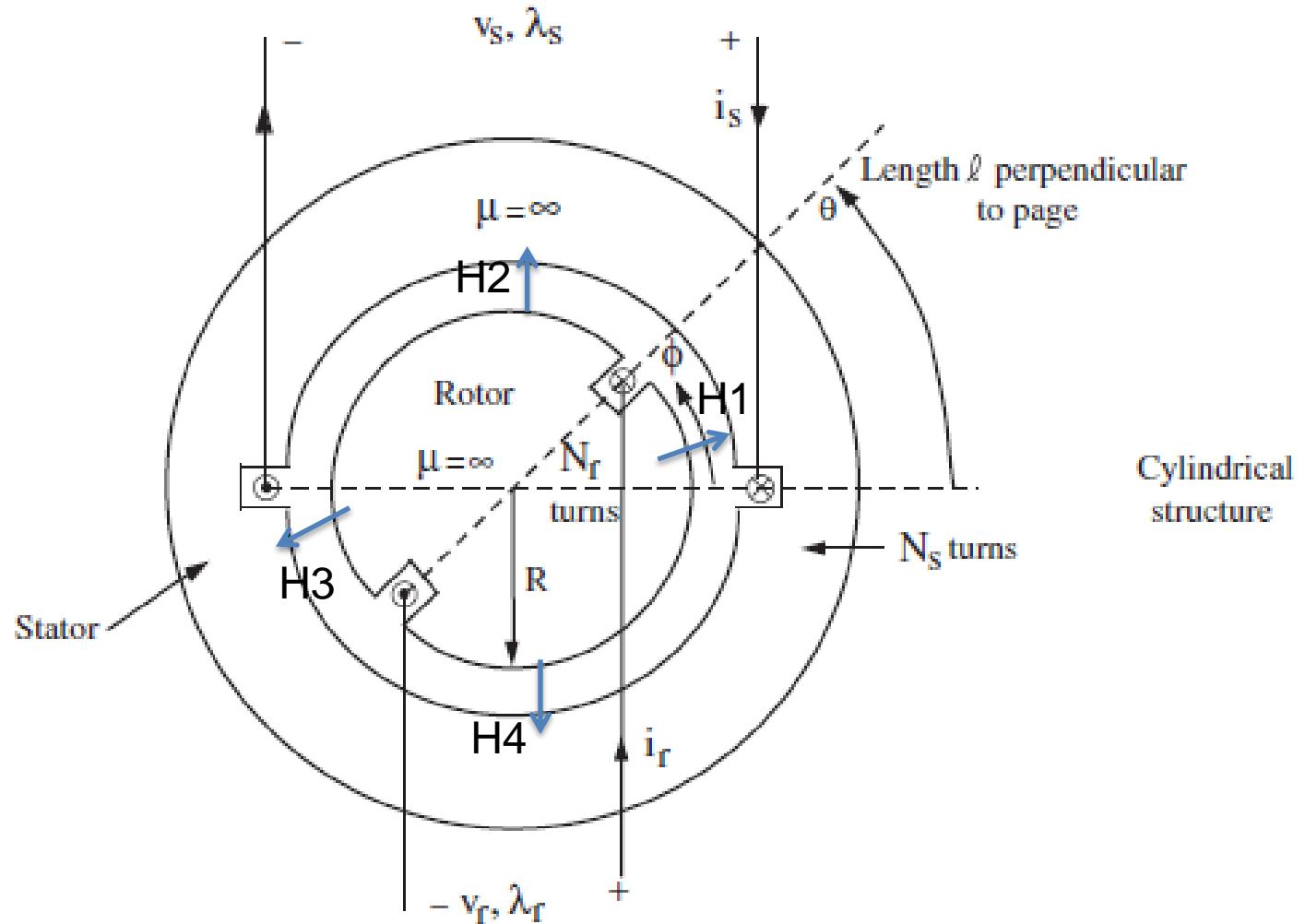
Find λ_s , λ_r as a function of i_s , i_r , and θ .

Also find v_s and v_r of the cylindrical rotor.



ROTATIONAL SYSTEM

Assume H is
constant in
each region



Cylindrical
structure

ROTATIONAL MECHANICAL SYSTEM

Four regions with different value of H :

$$0 < \phi < \theta \quad , \quad \theta < \phi < \pi \quad , \quad \pi < \phi < \pi + \theta \quad , \quad \pi + \theta < \phi < 2\pi$$

H_1 H_2 H_3 H_4

Ampere's circuital law

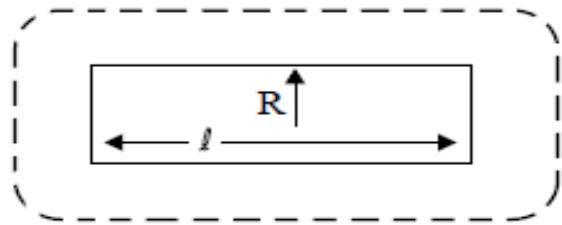
$$Contour \; 2 \qquad \qquad \qquad H_2 - H_1 = \frac{N_r i_r}{g} \dots \dots \dots (2)$$

$$Contour\ 3 \quad H_3 - H_2 = -\frac{N_s i_s}{g} \dots\dots\dots(3)$$

ROTATIONAL MECHANICAL SYSTEM

Gauss's law for magnetic fields

$$\oint_S B \bullet n da = 0$$



Multiplying by the circumferential area of each region

$$\mu_0 \ell R (H_1 \theta + H_2 (\pi - \theta) + H_3 \theta + H_4 (\pi - \theta)) = 0$$

$$\mu_0 \ell R [\theta(H_1 - H_2 + H_3 - H_4) + \pi(H_2 + H_4)] = 0$$

$$H_1 - H_2 + H_3 - H_4 = 0$$

ROTATIONAL MECHANICAL SYSTEM

Subtracting 2 from 1 and using 5

$$2H_1 = \frac{N_s i_s - N_r i_r}{g} \quad , \quad H_1 = \frac{N_s i_s - N_r i_r}{2g} = -H_3$$

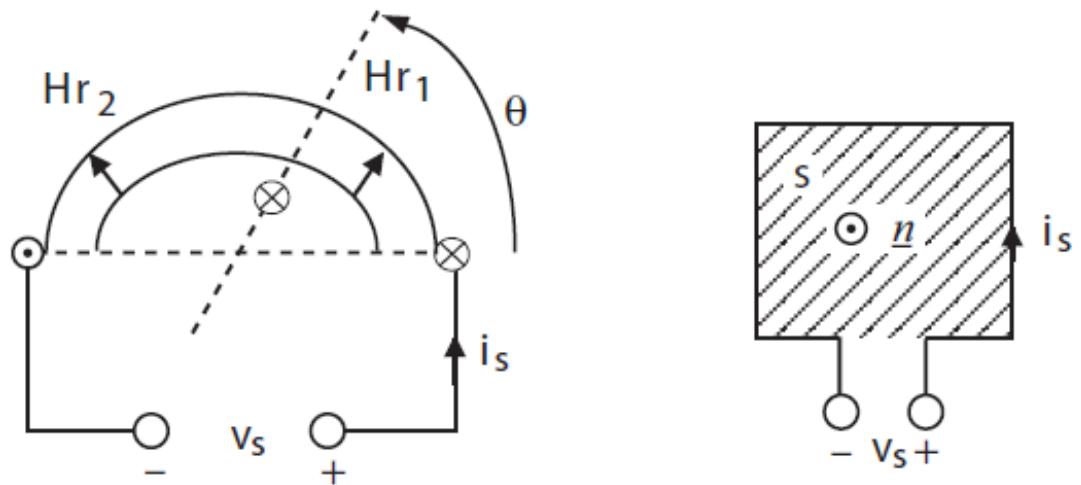
Subtracting 3 from 2 and using 6:

$$H_2 = \frac{N_s i_s + N_r i_r}{2g} = -H_4$$

ROTATIONAL MECHANICAL SYSTEM

STATOR FLUX LINKAGES

We first note that arc length of the coil with an angle θ is $R\theta$, where R is the radius



$$\begin{aligned}\phi_s &= \int_s \underline{B} \cdot \underline{n} da = \int_0^\theta \mu_o H_1 \ell R d\phi + \int_\theta^\pi \mu_o H_2 \ell R d\phi \\ &= (\mu_o H_1)(R\theta l) + (\mu_o H_2)(\pi - \theta)R l\end{aligned}$$

ROTATIONAL MECHANICAL SYSTEM

the flux through one turn of stator coil is

$$\lambda_s = N_s \phi_s = N_s \mu_o H_1 R \theta \ell + N_s \mu_o H_2 R (\pi - \theta) \ell$$

$$\lambda_s = \frac{N_s^2 \mu_0 R l \pi}{2g} i_s + N_s N_r \frac{\mu_0 R l \pi}{2g} \left(1 - \frac{2\theta}{\pi}\right) i_r$$

$$\lambda_s = N_s^2 L_0 i_s + N_s N_r L_0 \left(1 - \frac{2\theta}{\pi}\right) i_r, \quad L_0 = \frac{\mu_0 R l \pi}{2g}$$

$$\lambda_s = L_s i_s + L_m(\theta) i_r, \quad \text{where}$$

$$L_s = N_s^2 L_0, \quad L_m(\theta) = N_s N_r L_0 \left(1 - \frac{2\theta}{\pi}\right)$$

ROTATIONAL MECHANICAL SYSTEM

Rotor flux linkages:

$$\lambda_r = N_r \int_s B \bullet n da$$

$$= N_r \int_{\theta}^{\pi} \mu_0 H_2 \ell R d\phi + N_r \int_{\pi}^{\pi+\theta} \mu_0 H_3 \ell R d\phi$$

$$\lambda_r = N_r \mu_0 H_2 \ell R (\pi - \theta) + N_r \mu_0 H_3 \ell R \theta$$

$$\lambda_r = N_r \mu_0 \frac{N_s i_s + N_r i_r}{2g} R \ell (\pi - \theta) - N_r \mu_0 \frac{N_s i_s - N_r i_r}{2g} R \ell \theta$$

ROTATIONAL MECHANICAL SYSTEM

$$\begin{aligned}\lambda_r &= N_r \mu_0 \frac{N_s i_s}{2g} R \ell \pi - N_r \mu_0 \frac{N_s i_s}{2g} R \ell \theta + N_r \mu_0 \frac{N_r i_r}{2g} R \ell \pi - \frac{N_r i_r}{2g} R \ell \theta \\ &\quad - N_r \mu_0 \frac{N_s i_s}{2g} R \ell \theta + N_r \mu_0 \frac{N_r i_r}{2g} R \ell \theta \\ \lambda_r &= N_s N_r L_0 \left(1 - \frac{2\theta}{\pi} \right) i_s + N_r^2 L_0 i_r \\ &= L_m(\theta) i_s + L_r i_r\end{aligned}$$

Note: $L_r = N_r^2 L_0$

INDUCTANCE IN THE ROTATIONAL EXAMPLE

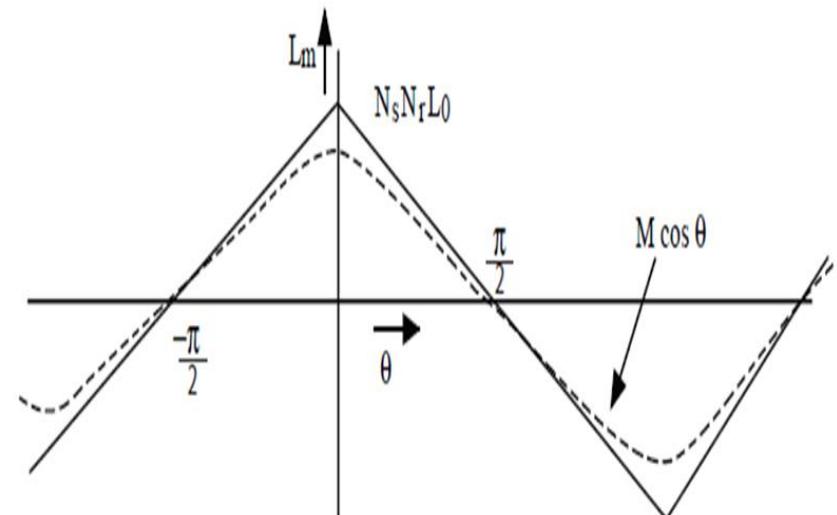
- The flux linkages are

$$\lambda_s = L_s i_s + L_m(\theta) i_r$$

$$\lambda_r = L_r i_r + L_m(\theta) i_s$$

The actual mutual inductance is a triangular wave, but is usually approximated as a sine wave.

$$L_m = M \cos(\theta).$$



ROTATIONAL MECHANICAL SYSTEM

If:

$$L_m = M \cos \theta$$

$$v_s = \frac{d \lambda_s}{dt} = L_s \frac{di_s}{dt} + M \cos \theta \underbrace{\frac{di_r}{dt} - i_r M \sin \theta \frac{d\theta}{dt}}_{\text{Speed voltage}}$$

$$v_r = \frac{d \lambda_r}{dt} = L_r \frac{di_r}{dt} + M \cos \theta \underbrace{\frac{di_s}{dt} - i_s M \sin \theta \frac{d\theta}{dt}}_{\text{Speed voltage}}$$

LINEAR SYSTEMS

- A linear system can be formulated based on the flux linkage and current equations.

$$\begin{bmatrix} i_s \\ i_r \end{bmatrix} = \begin{bmatrix} L_s & L_m(\theta) \\ L_m(\theta) & L_r \end{bmatrix}^{-1} \begin{bmatrix} \lambda_s \\ \lambda_r \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} i_s \\ i_r \end{bmatrix} = \frac{1}{L_s L_r - L_m^2(\theta)} \begin{bmatrix} L_r & -L_m(\theta) \\ -L_m(\theta) & L_s \end{bmatrix} \begin{bmatrix} \lambda_s \\ \lambda_r \end{bmatrix}$$