

ECE 330

POWER CIRCUITS AND ELECTROMECHANICS

LECTURE 22

INDUCTION MACHINES (3)

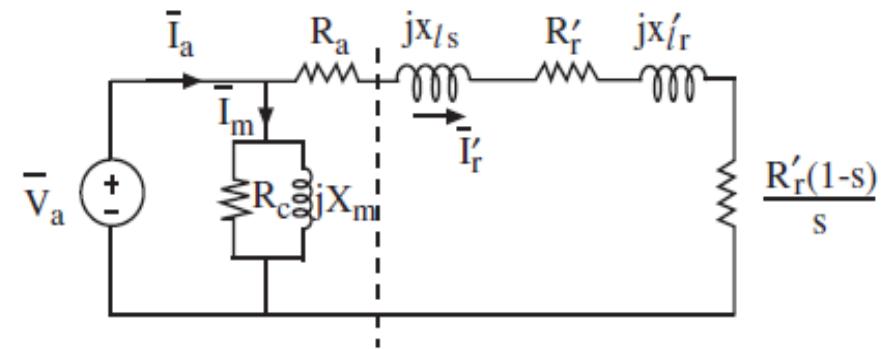
Acknowledgment-These handouts and lecture notes given in class are based on material from Prof. Peter Sauer's ECE 330 lecture notes. Some slides are taken from Ali Bazi's presentations

Disclaimer- These handouts only provide highlights and should not be used to replace the course textbook.

EXPRESSION FOR T^e IN TERMS OF V_a

Using approximate per-phase equivalent circuit:

$$\bar{I}'_r = \frac{\bar{V}_a}{(R_a + \frac{R'_r}{s}) + j(X_{\ell s} + X'_{\ell r})}$$



The magnitude of the current \bar{I}'_r

$$I'_r = \frac{V_a}{\sqrt{(R_a + \frac{R'_r}{s})^2 + (X_{\ell s} + X'_{\ell r})^2}}$$

$$P_m = 3(I'_r)^2 R'_r \frac{(1-s)}{s} = \frac{3V_a^2 R'_r \frac{(1-s)}{s}}{(R_a + \frac{R'_r}{s})^2 + (X_{\ell s} + X'_{\ell r})^2}$$

EXPRESSION FOR T^e IN TERMS OF V_a

For the two-pole machine $\omega_m = \omega_s (1 - s)$

$$P_m = T^e \omega_m = T^e \omega_s (1 - s)$$

$$T^e = \frac{P_m}{\omega_s (1 - s)}$$

$$T^e = \frac{3V_a^2 \frac{R_r'}{s \omega_s}}{(R_s + \frac{R_r'}{s})^2 + (X_{\ell s} + X'_{\ell r})^2} = f(V_a, s)$$

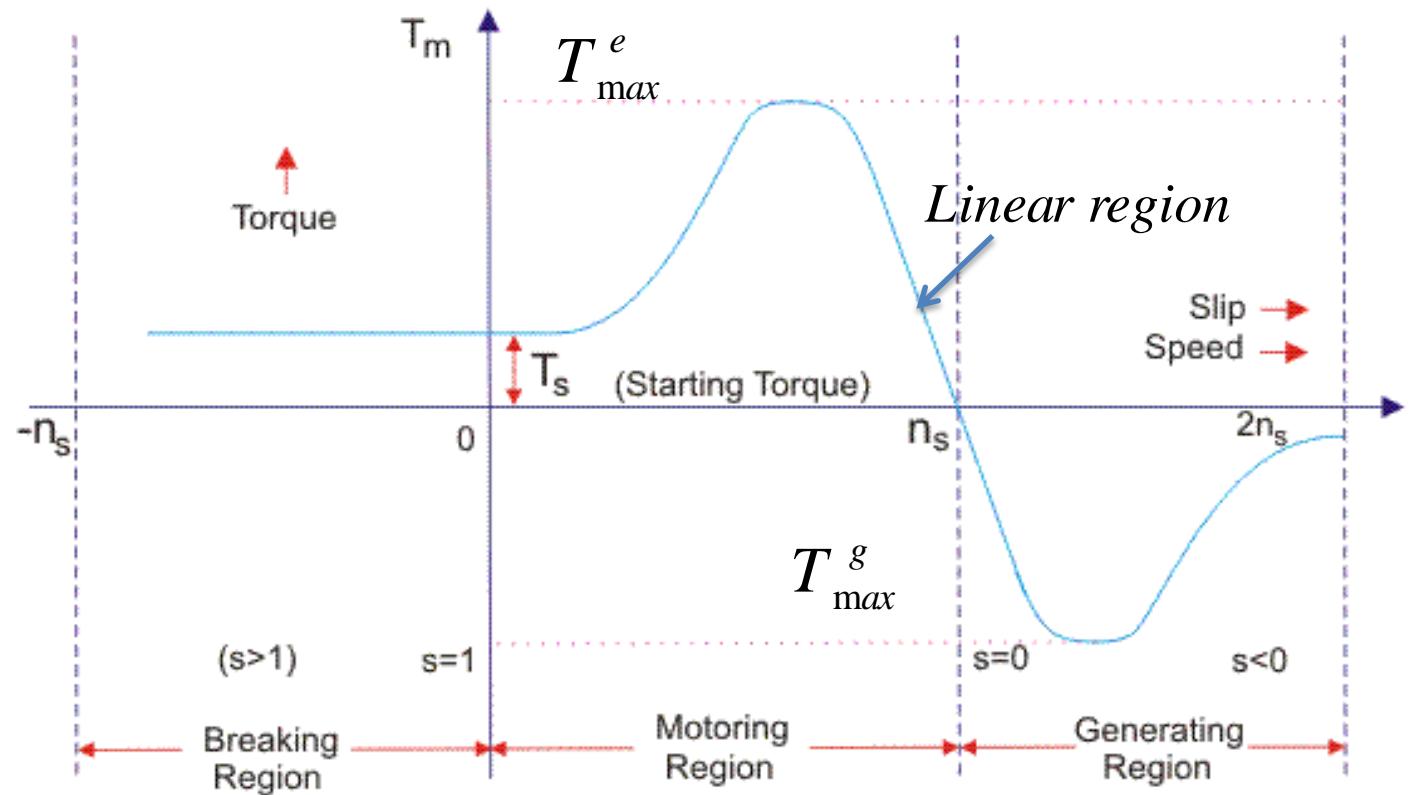
TORQUE-SPEED CURVE

T^e can be approximated as

$$T^e = \frac{P_{ag}}{\omega_s \frac{2}{P}} = \frac{3I_r'^2 \frac{R_r'}{s}}{\omega_s \frac{2}{P}}$$

Note: T^e is max. when P_{ag} is max.

TORQUE-SPEED CURVE



$0 < s < 1 \Rightarrow Motor$

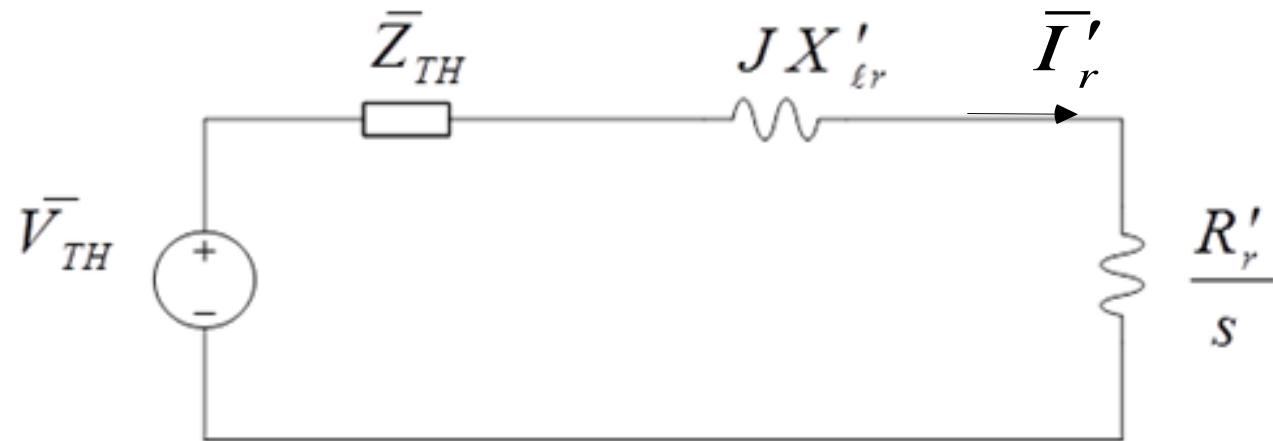
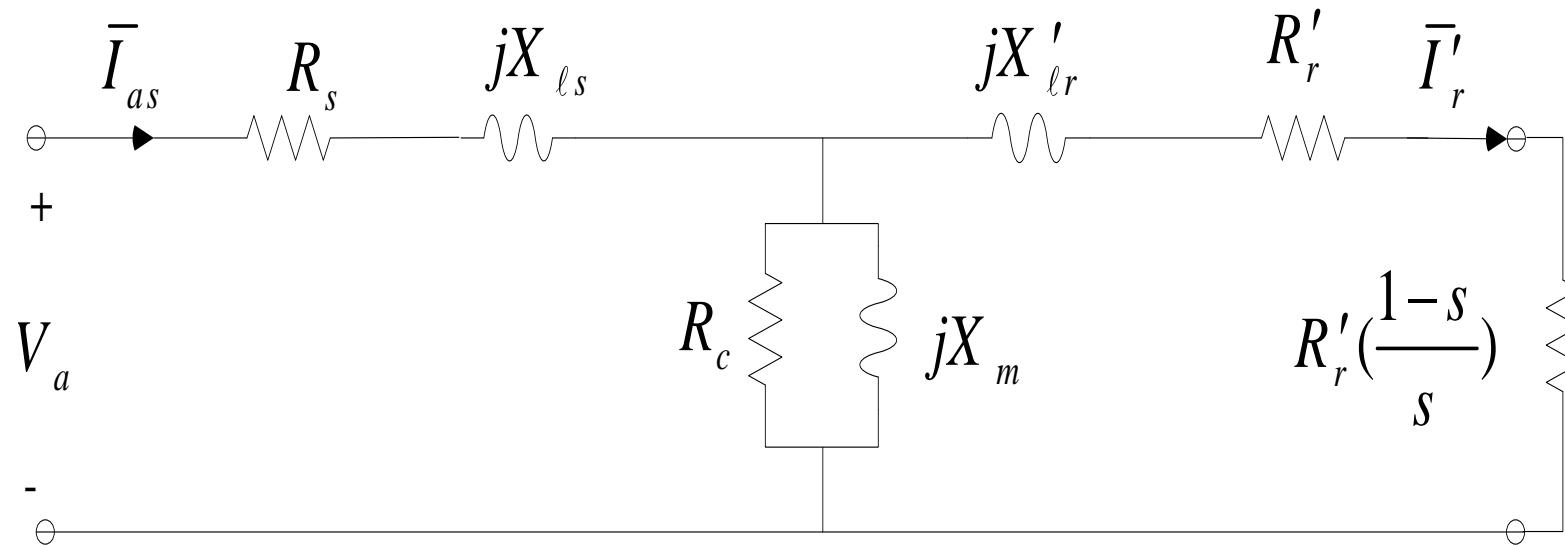
$s < 0 \Rightarrow Generator$

$1 < s < 2 \Rightarrow Breaking$

Torque Slip Curve for Three Phase Induction Motor

Source:electrical4u.com

USING THEVENIN THEORY



USING THEVENIN THEORY

$$p_{ag} = 3|I'_r|^2 \frac{R'}{s}$$

$$\left| I'_r \right| = \left| \frac{V_{TH}}{Z_{TH} + \frac{R'_r}{s} + jX'_{\ell r}} \right|$$

$$P_{ag} = \frac{3 |V_{TH}|^2 \frac{R'_r}{s}}{(R_{TH} + \frac{R'_r}{s})^2 + (X_{TH} + X'_{\ell r})^2}$$

$$T^e = \frac{P_m}{\omega_m} = \frac{P_{ag}(1-s)}{(1-s)\omega_s} = \frac{P_{ag}}{\omega_s}$$

USING THEVENIN THEORY

$$T^e = \frac{3 |V_{TH}^-|^2 \frac{R'_r}{s}}{\omega_s \frac{2}{P} [(R_{TH} + \frac{R'_r}{s})^2 + (X_{TH} + X'_{\ell r})^2]}$$

$$T^e = \frac{3 |V_{TH}^-|^2 R'_r s}{\omega_s \frac{2}{P} [(R_{TH} s + R'_r)^2 + s^2 (X_{TH} + X'_{\ell r})^2]}$$

For small slip (*so* $R_{TH} s \ll R'_r$ and $s^2 (X_{TH} + X'_{\ell r})^2 \ll R'^2_r$)

$$T^e = \frac{3 |V_{TH}^-|^2}{\omega_s \frac{2}{P} R'_r} s$$

EXPRESSION FOR MAXIMUM TORQUE

$$T^e = \frac{3V_a^2 \frac{R'_r}{s\omega_s}}{(R_s + \frac{R'_s}{s})^2 + (X_{\ell s} + X'_{\ell r})^2} = f(V_a, s)$$

For T^e to have maximum value, $\frac{dT^e}{ds} = 0$

$$\frac{R'_r}{s} = \sqrt{R_a^2 + (x_{\ell s} + x'_{\ell r})^2}$$

The slip at which maximum torque occurs

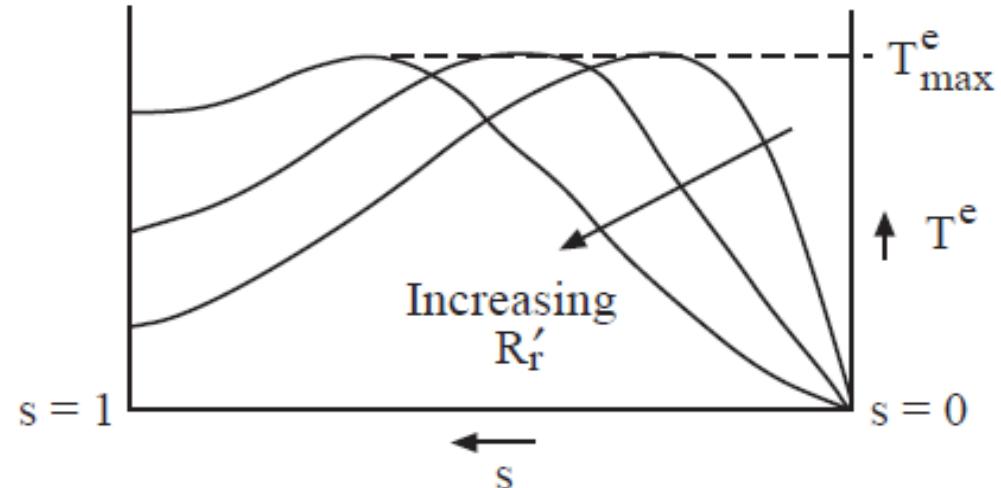
$$s_{mT} = \frac{R'_r}{\sqrt{R_a^2 + (x_{\ell s} + x'_{\ell r})^2}}$$

EXPRESSION FOR MAXIMUM TORQUE

In special case when $R_a = 0$

$$s_{mT} = \frac{R'_r}{(x_{\ell s} + x'_{\ell r})}$$

$$T^e_{\max} = \frac{3}{2} \frac{V_a^2}{\omega_s (x_{\ell s} + x'_{\ell r})}$$



T^e_{\max} is independent of the rotor resistance, but s_{mT} is dependent on the value of R'_r .

The maximum value of T^e is the same but it occurs at different values of s depending on R'_r

MULTI-POLE INDUCTION MACHINES

For a p pole machine, we can repeat the analysis with mechanical angle θ substituted by $\left(\frac{p}{2}\right)\theta$

$$\omega_r = \omega_s - \left(\frac{p}{2}\right)\omega_m \quad , \quad s = \frac{\omega_s - (p/2)\omega_m}{\omega_s} \quad , \quad \omega_m = \frac{\omega_s(1-s)}{p/2}$$

Mechanical power P_m is given by $P_m = T^e \omega_m = T^e \frac{\omega_s(1-s)}{(p/2)}$

$$T^e = \left(\frac{p}{2}\right) 3V_a^2 \frac{R'_r}{s\omega_s} / \left[\left(R_a + \frac{R'_r}{s} \right)^2 + (x_{\ell s} + x'_{\ell r})^2 \right] = f(V_a, s)$$

$$T_{max}^e = \left(\frac{p}{2}\right) \frac{3}{2} \frac{V_a^2}{\omega_s (x_{\ell s} + x'_{\ell r})} \quad , \quad T_{max}^e = \left(\frac{p}{2}\right) \frac{3}{2} \frac{V_{th}^2}{\omega_s (x_{th} + x'_{\ell r})}$$

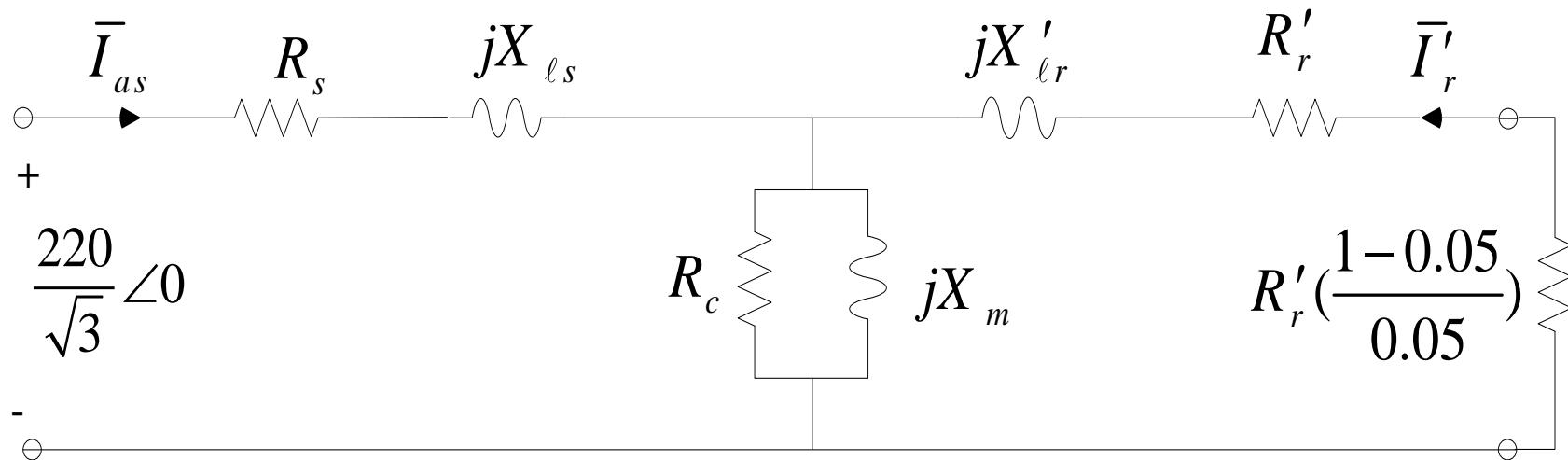
PROBLEM 7.4

A three-phase, four pole, 60 Hz, 30 hp, 220 V, wye connected induction motor draws a current of 77 A from the line source at a P.F. of 0.88 *lagging*. $s = 0.05$, $P_{sc\ell} = 1033W$, $P_c = 485W$

Find:

- (a) the power across air gap P_{ag} .
- (b) T^e torque of electric origin.
- (c) P_m mechanical power delivered to shaft.
- (d) actual horsepower developed and the overall efficiency if rotational losses are 540 W.

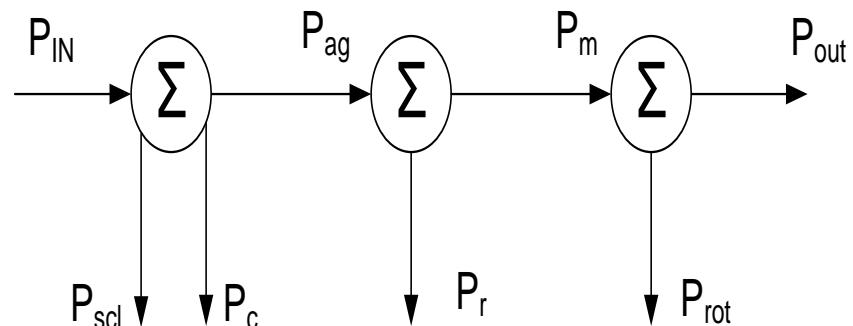
PROBLEM 7.4



$$(a): P_{IN} = 3 \times \frac{220}{\sqrt{3}} \times 77 \times 0.88 = 25821 \text{ W}$$

$$P_{ag} = P_{IN} - P_{sc\ell} - P_c = 24303 \text{ W}$$

$$(b): T^e = \frac{P_{ag}}{\omega_s \frac{2}{P}} = \frac{24303}{2\pi 60 \times \frac{2}{4}} = 129 \text{ N-m}$$



PROBLEM 7.4

$$(c): \quad P_m = (1 - s)P_{ag} = 0.95 \times 24303 = 23088 \text{ W}$$

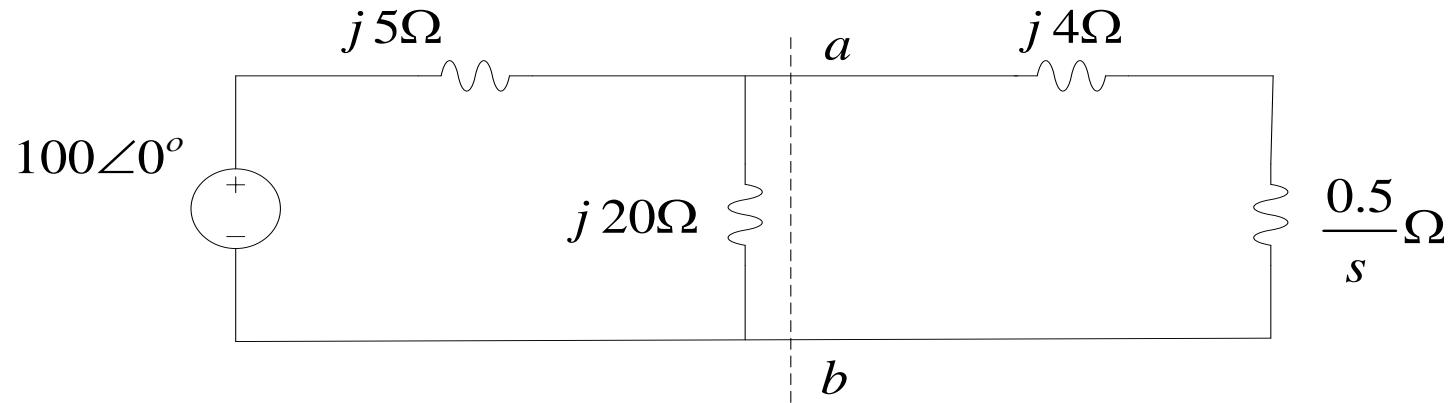
$$P_{out} = P_{shaft} = P_m - P_{rot} = 23088 - 540 = 22548 \text{ W}$$

$$(d): \quad \text{Actual hp} = \frac{P_{out}}{746} = \frac{22548}{746} = 302 \text{ hp}$$

$$\mu = \frac{P_{out}}{P_{IN}} \times 100 = \frac{22548}{25821} \times 100 = 87\%$$

PROBLEM 7.12

The per-phase equivalent circuit of a three-phase, four-pole, 60 Hz induction motor is given in the figure below.

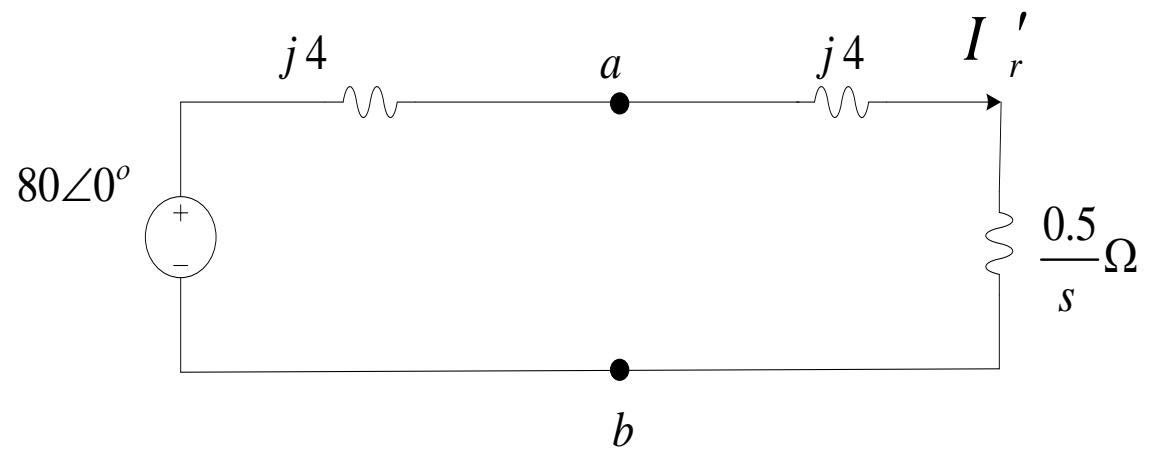


- (a): Find T^e using the Thevenin equivalent to the left of the dotted line.
- (b): Find T_{\max}^e , s_{mT} , and T_{starting}^e .

PROBLEM 7.12

$$\bar{V}_{TH}^{ab} = j20 \left(\frac{100\angle 0^\circ}{j25} \right) = 80\angle 0^\circ$$

$$\bar{Z}_{TH} = \frac{j5 \times j20}{j25} = j4$$



$$I_r' = \frac{80\angle 0^\circ}{\frac{0.5}{s} + j8} = \frac{80(s)}{0.5 + j8(s)}$$

PROBLEM 7.12

$$T^e = \frac{3|I_r'|^2 \frac{0.5}{s}}{2\pi 60X \frac{2}{4}} = \frac{3X \cdot 6400(s)^2 \left(\frac{0.5}{s}\right)}{2\pi 30X \cdot (0.25 + 64(s)^2)} = \frac{51(s)}{0.25 + 64(s^2)}$$

$$s_{T_{\max}} = \frac{0.5}{8} = 0.0625$$

(b) $T_{\max}^e = 6.4 \text{ N-m}$

$$T_{start}^e = T^e \Big|_{s=1} = 0.8 \text{ N-m}$$