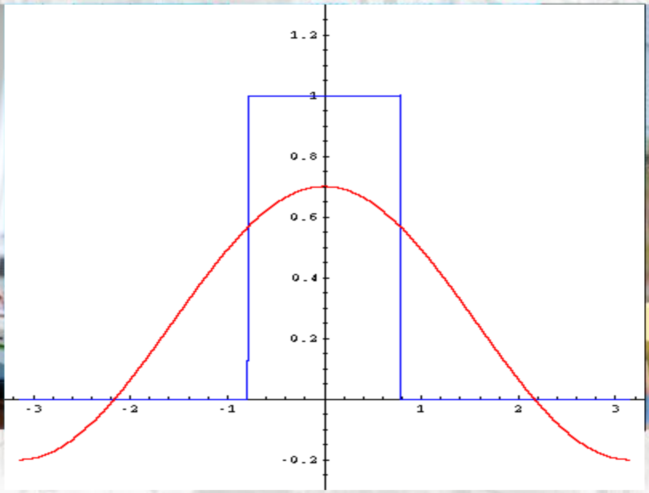
Frequency domain analysis of linear circuits using synchronous detection

Physics 401, Spring 2014.

Eugene V. Colla



Frequency domain analysis of linear circuits using synchronous detection

Outline

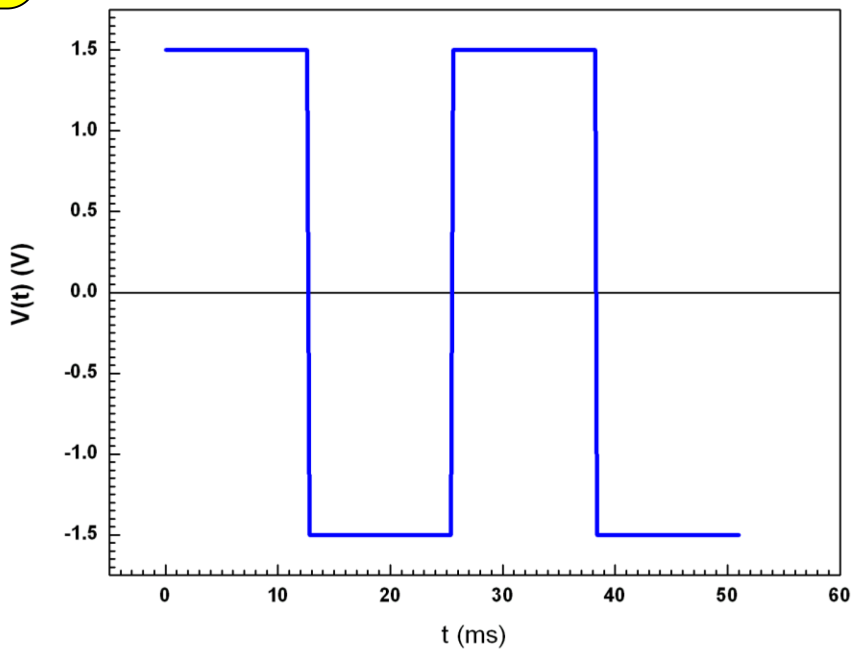
1. Fourier transform,. Discrete Fourier transform. Some properties.
2. Time domain and Frequency domain representation of the data.
3. Frequency domain spectroscopy (FDS)
4. Lock-in amplifiers
5. Practical application of lock-in’s in FDS
6. Taking data and simple data analysis using OriginPro.

in 1822, Jean Baptiste Fourier developed the theory that shows that any real waveform can be represented by the sum of sinusoidal waves.

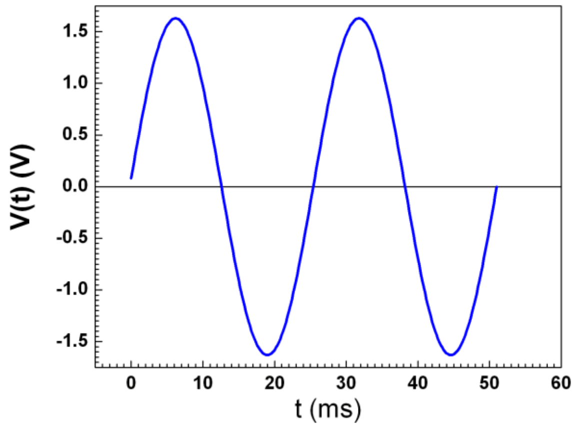
Jean Baptiste Joseph Fourier (1768 – 1830)

Let we try to create the square wave as a sum of sine waves of different frequencies

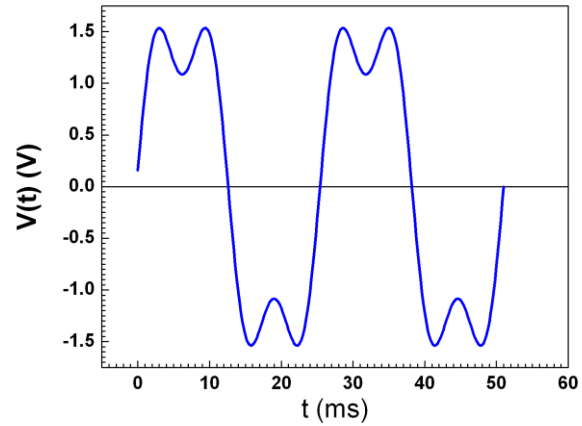
Square wave.
F=40Hz, A=1.5V



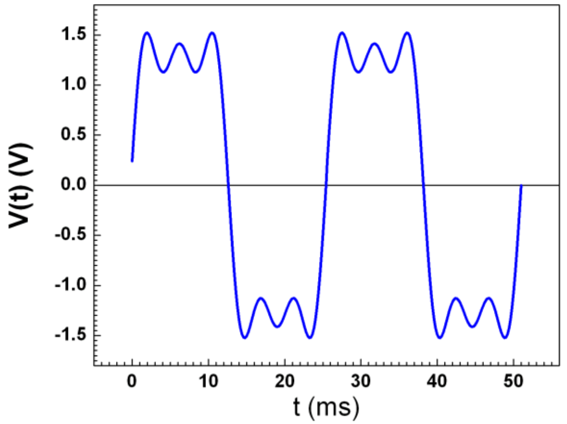
$A_1 \sin(2\pi\omega t)$



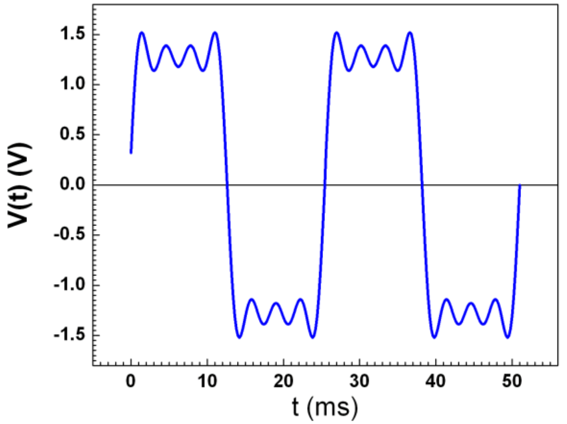
$A_1 \sin(2\pi\omega t) + A_3 \sin(2\pi 3\omega t + \varphi_3)$



$A_1 \sin(2\pi\omega t) + A_3 \sin(2\pi 3\omega t + \varphi_3) +$
$A_5 \sin(2\pi 5\omega t + \varphi_5)$



$A_1 \sin(2\pi\omega t) + A_3 \sin(2\pi 3\omega t + \varphi_3) +$
$A_5 \sin(2\pi 5\omega t + \varphi_5) + A_7 \sin(2\pi 7\omega t + \varphi_7)$



Fourier Transform

The continues Fourier transformation of the signal h(t) can be written as:

$$H(f)=\int_{-\infty}^{+\infty} h(t)e^{2\pi jft}dt; \quad j=\sqrt{-1}$$

H(f) represents in frequency domain mode the time domain signal h(t)

Equation for inverse Fourier transform gives the correspondence of the infinite continues frequency spectra to the corresponding time domain signal.

$$h(t)=\int_{-\infty}^{+\infty} H(f)e^{-2\pi jft}df$$

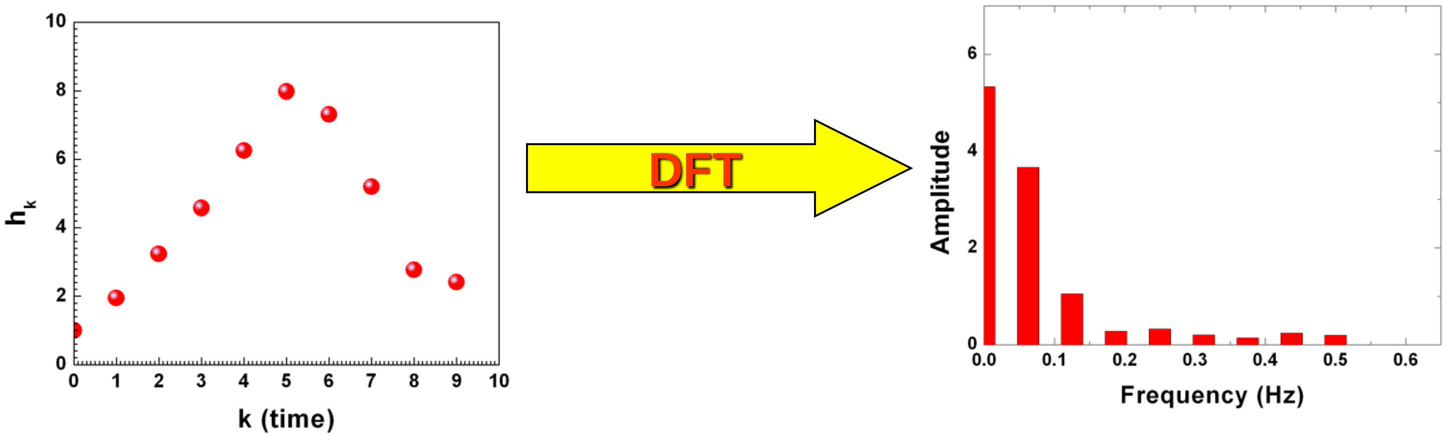
In real life we working with discrete representation of the time domain signal recorded during a finite time.

Discrete Fourier Transform

It comes out that in practice more useful is the representation the frequency domain pattern of the time domain signal h_k as sum of the frequency harmonic calculated as:

$$H_n = H(f_n) = \frac{1}{N}\sum_{k=0}^{N-1} h_k e^{2\pi kn/N}$$

Δ is the sampling interval, N – number of collected points



Time domain **Frequency domain**

Discrete Fourier Transform

For periodic signals with period T_0:

$$F(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} a_n \cos\left(\frac{2\pi nt}{T_0}\right) + \sum_{n=1}^{\infty} b_n \sin\left(\frac{2\pi nt}{T_0}\right)$$

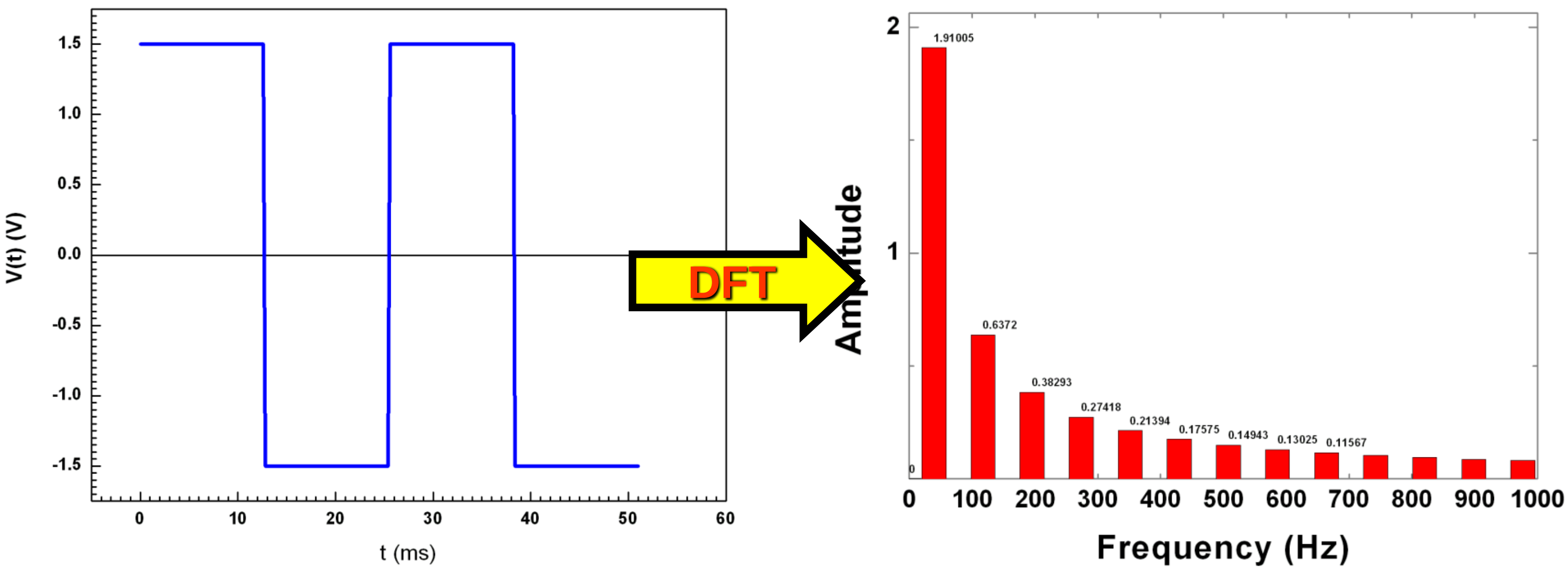
$$a_n = \frac{2}{T_0}\int_0^{T_0} F(t)\cos\left(\frac{2\pi nt}{T_0}\right)dt; \qquad b_n = \frac{2}{T_0}\int_0^{T_0} F(t)\sin\left(\frac{2\pi nt}{T_0}\right)dt;$$

$$a_0 = \frac{2}{T_0}\int_0^{T_0} F(t)dt;$$

Discrete Fourier Transform

Now how I found the amplitudes of the harmonics to compose the square wave signal from sine waves of different frequencies.

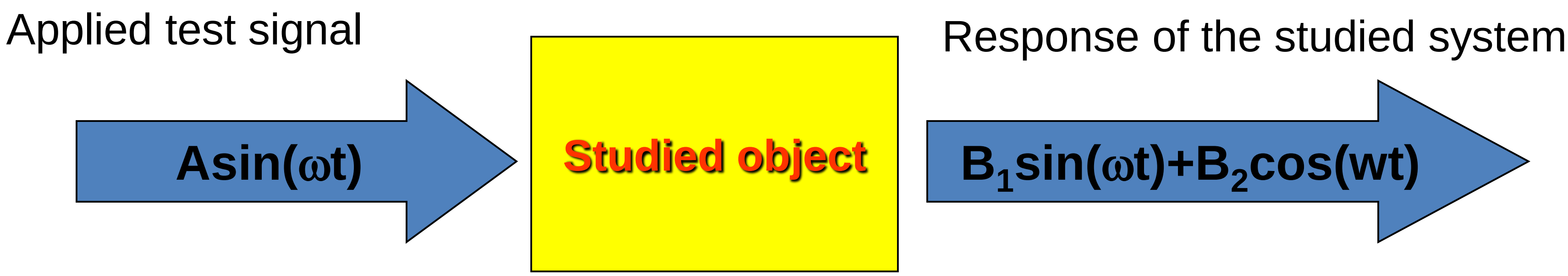
Time domain signal



Decomposition the signal into the sine wave harmonics. The only modulus's of the harmonics amplitudes are presented in this picture.

Frequency Domain Spectroscopy

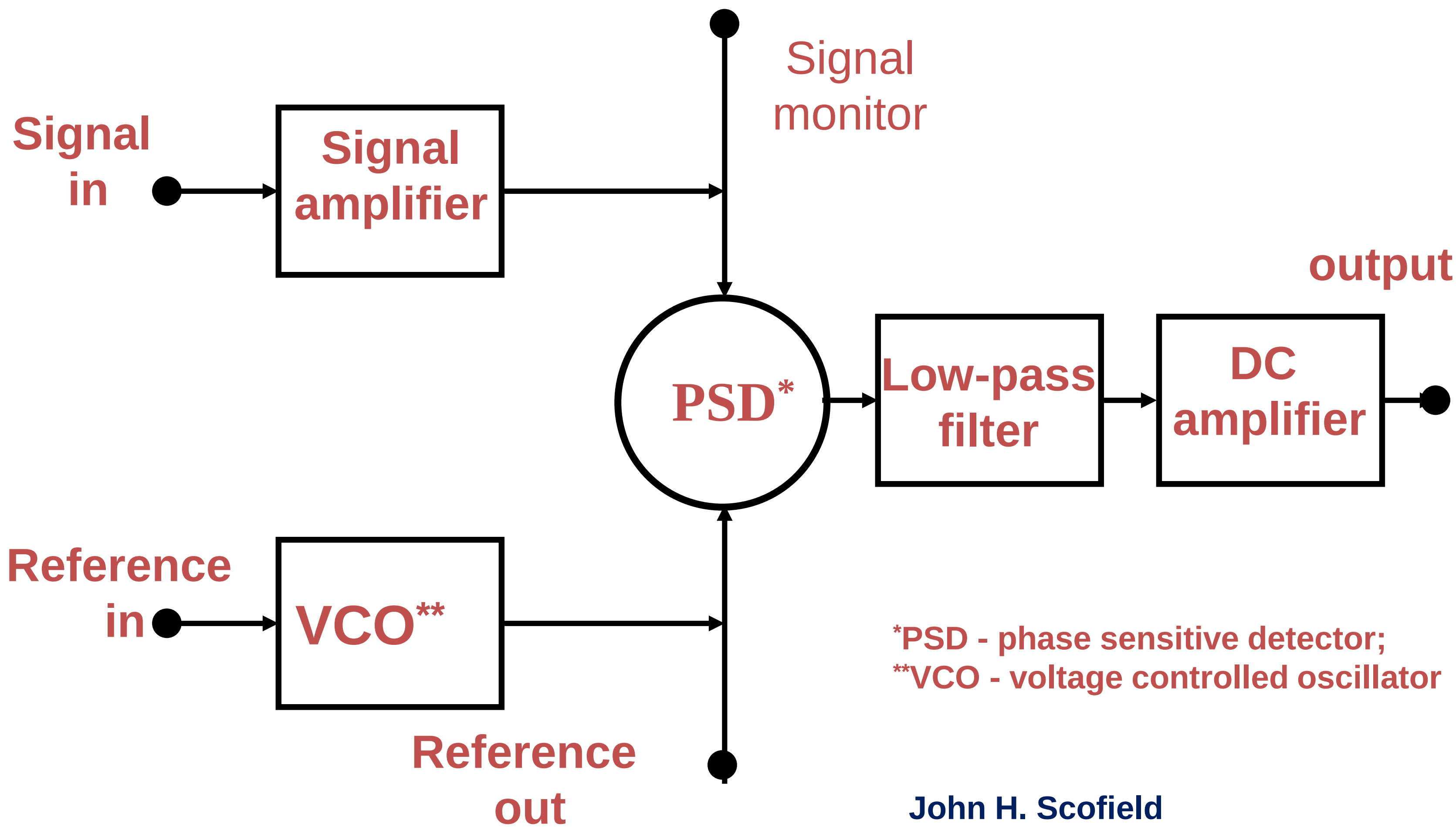
(linear system)



We applying the sine wave signal to tested object and measuring the response. Varying the frequency we can study the frequency properties of the system

Lock-in amplifier

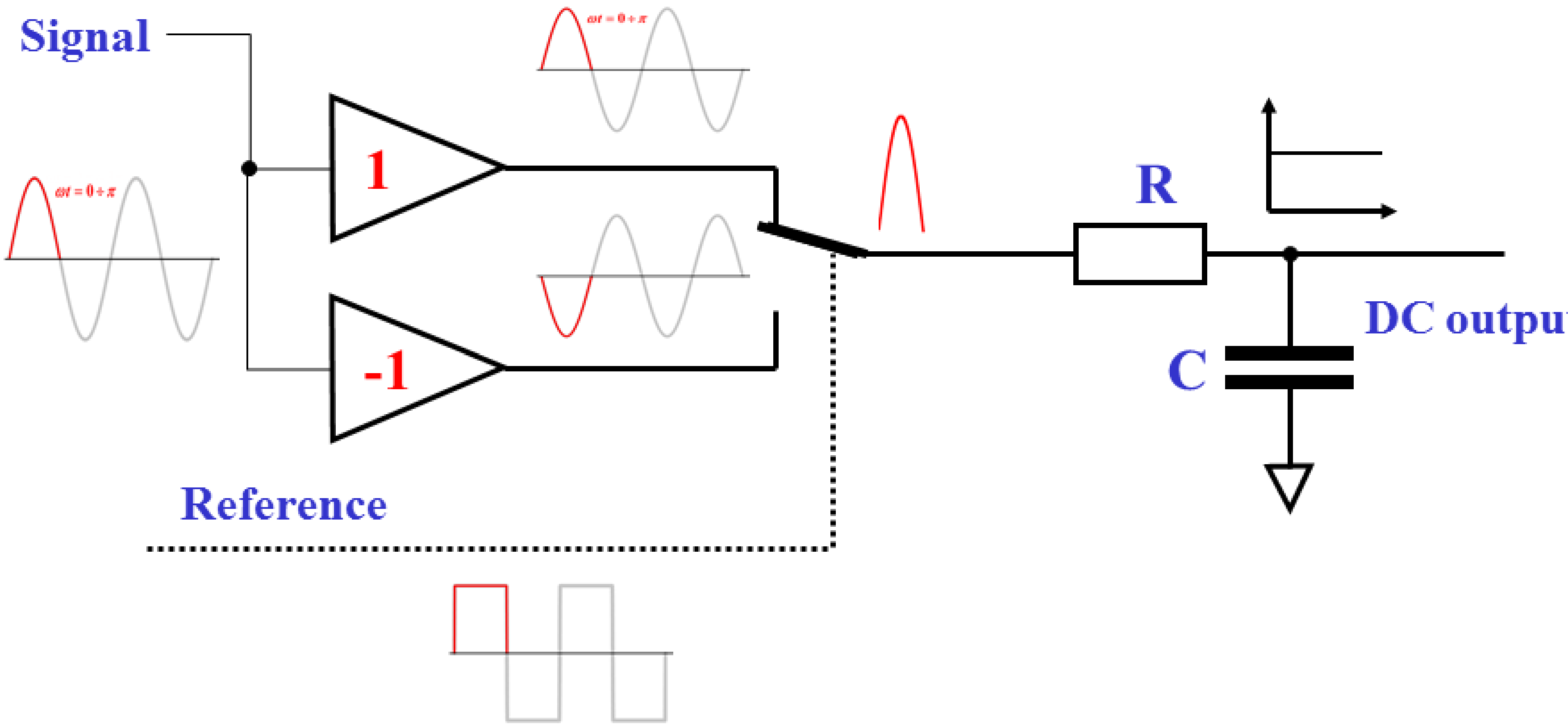
Now about the most powerful tool which can be used in frequency domain technique.



*PSD - phase sensitive detector;
**VCO - voltage controlled oscillator

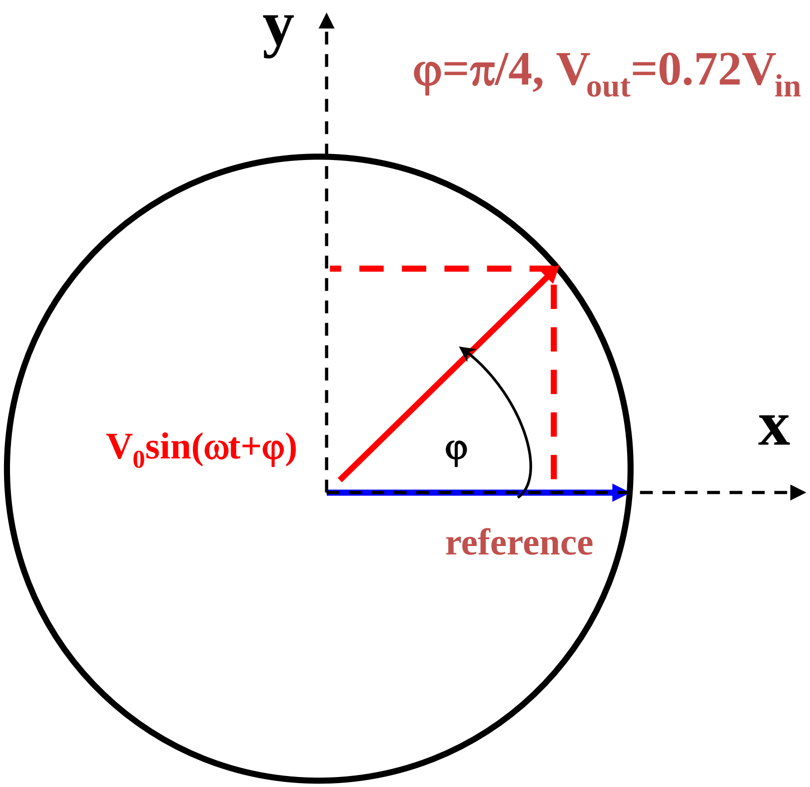
John H. Scofield
American Journal of Physics 62 (2) 129-133 (Feb. 1994).

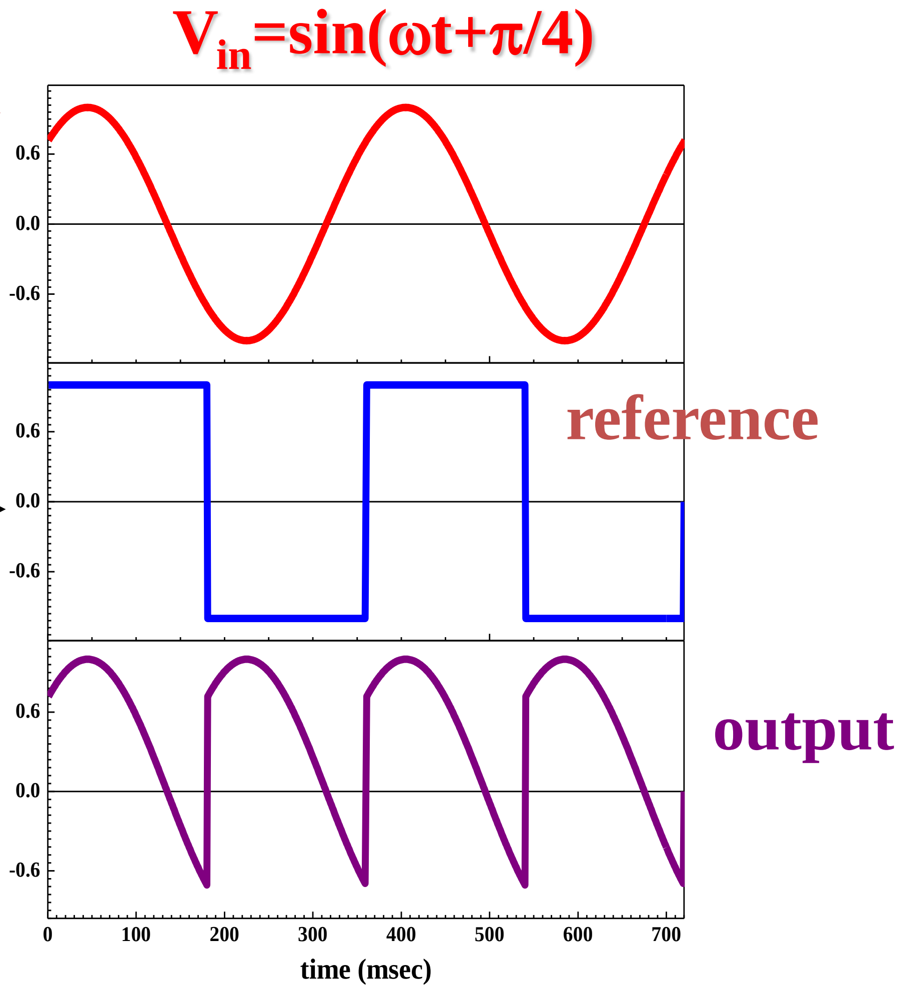
Lock-in amplifier. How it works.



The DC output signal is a magnitude of the product of the input and reference signals. AC components of output signal are filtered out by the low-pass filter with time constant τ (her τ=RC)

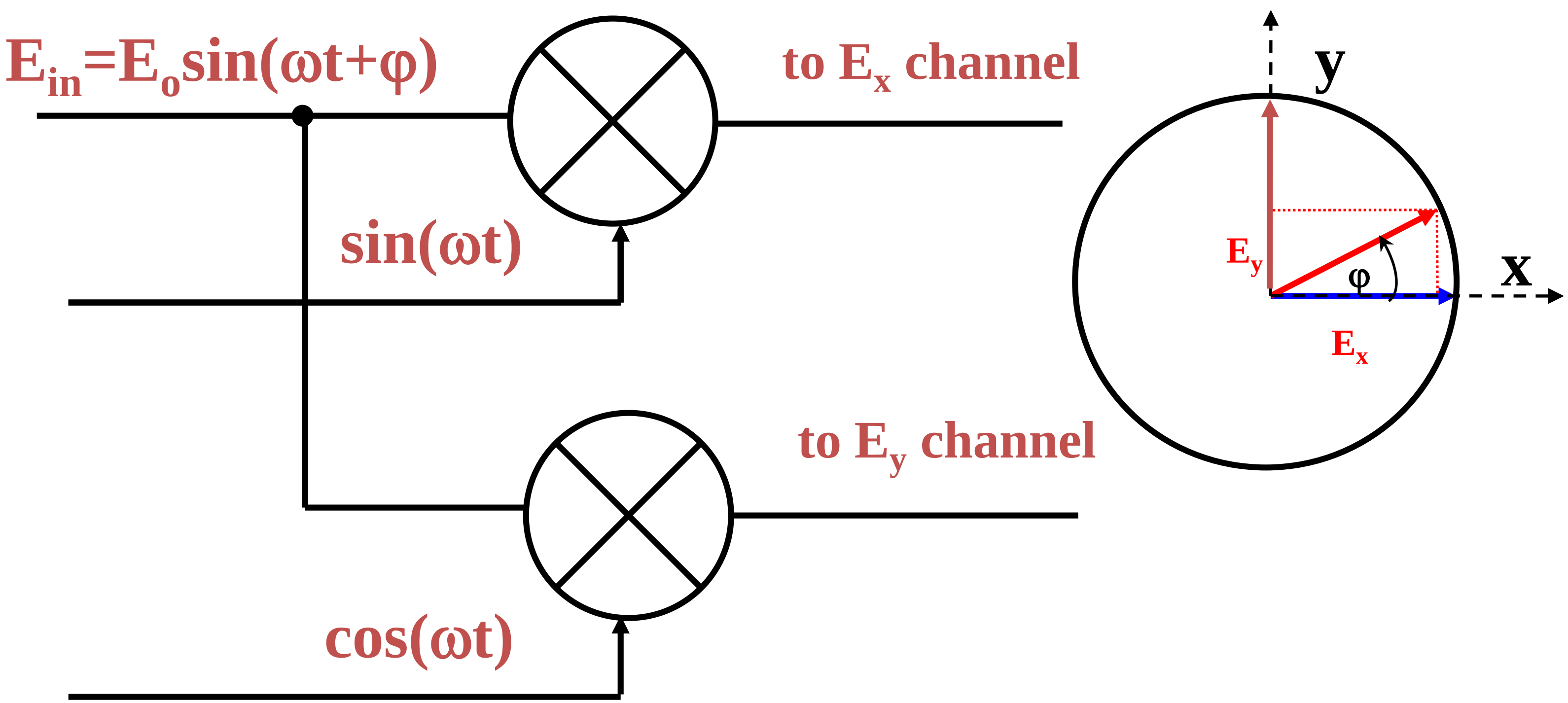
Lock-in amplifier. Phase shift.



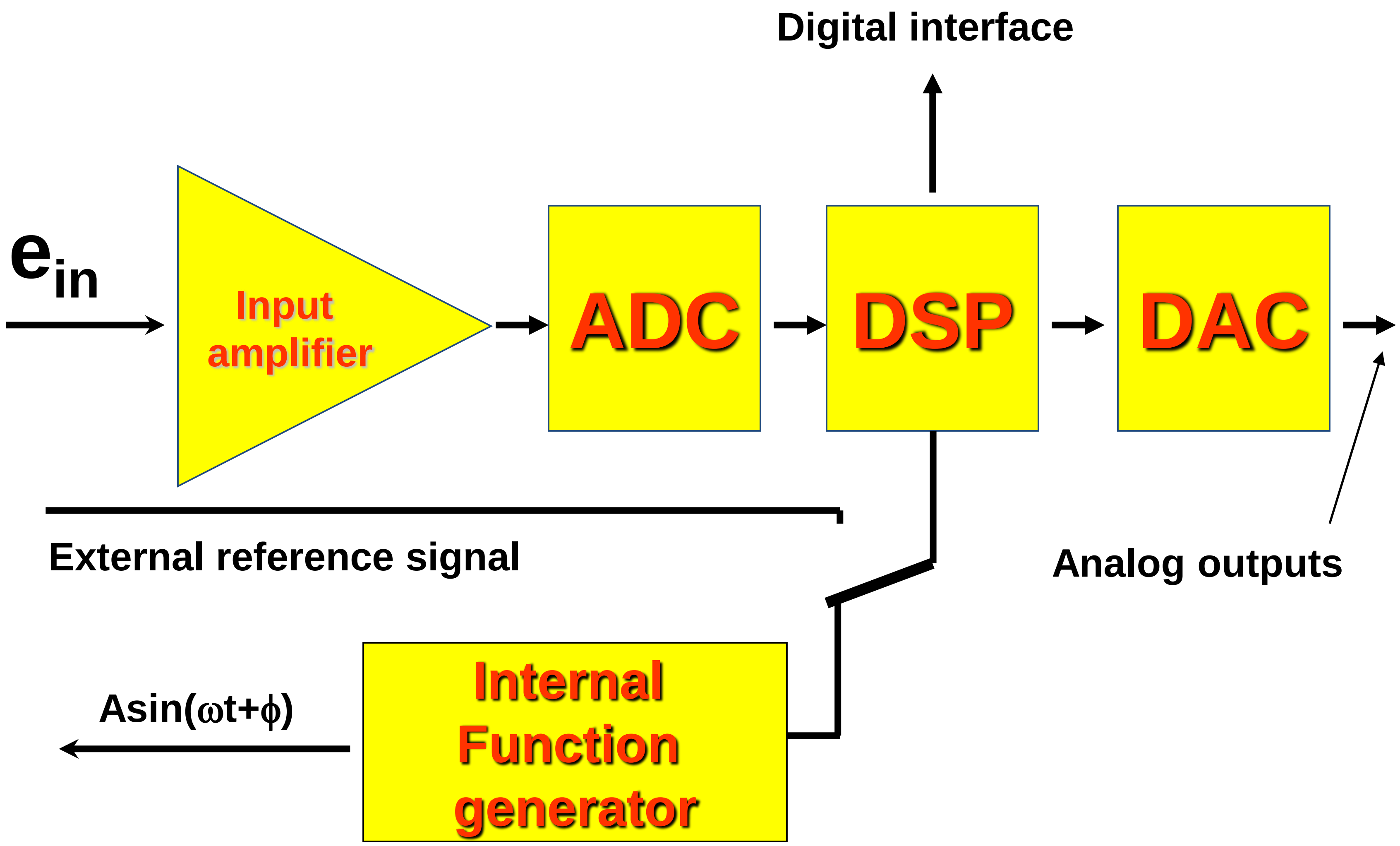


Lock-in amplifier. Two channels demodulation.

In many scientific applications it is a great advantage to measure both components (E_x, E_y) of the input signal. We can use two lock-ins to do this or we can measure these value in two steps providing the phase shift of reference signal 0 and π/4. Much better solution is to use the lock-in amplifier equipped by two demodulators.



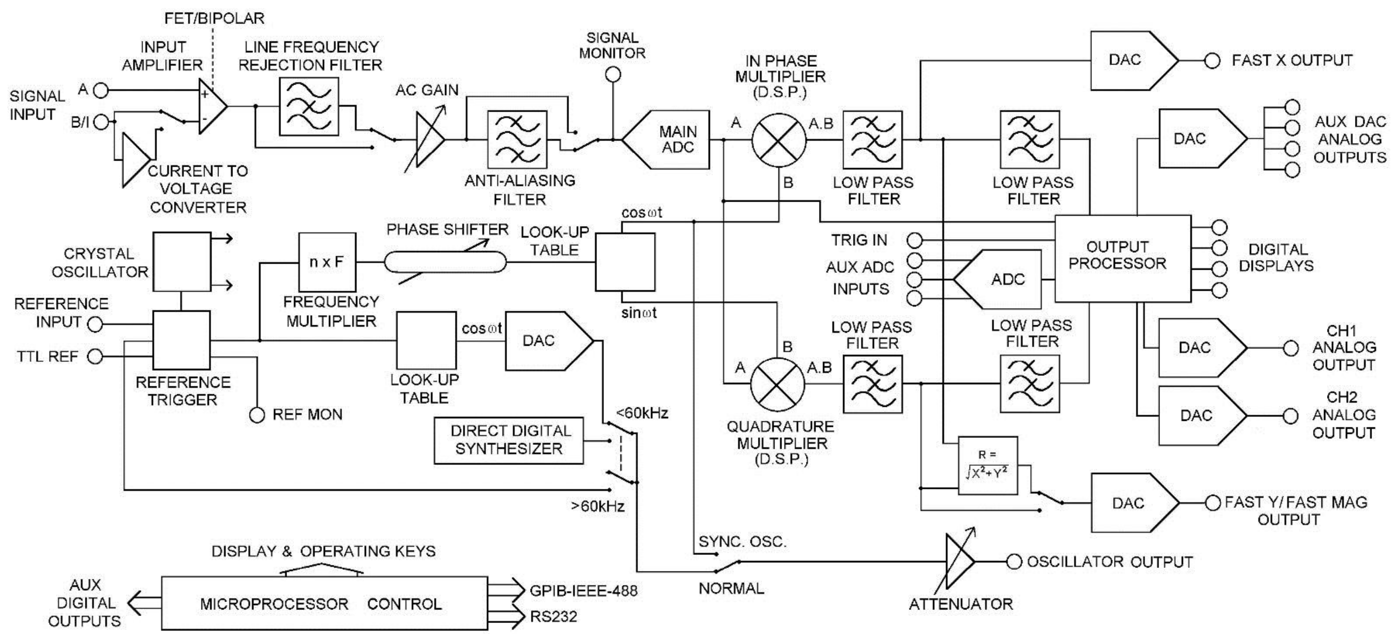
Digital Lock-in amplifier



Digital Lock-in amplifier

Digital lock-in SR830

[Lock-in demo]



Digital Lock-in amplifier. SR830

Time constant
And output filter

sensitivity

Auto functions

Channel#1

Channel#2

Inputs

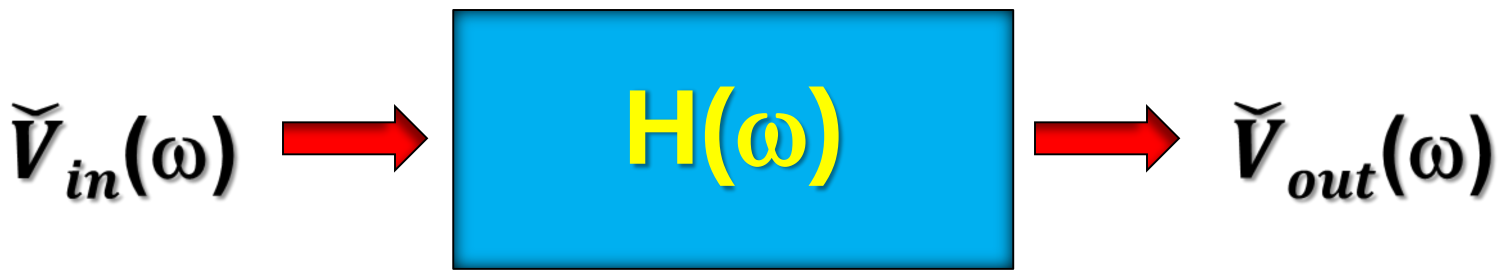
Notch
filter
settings

Analog outputs

Interface
settings

Function
generator

Experiments. Main idea.
Investigating the frequency response of circuit.

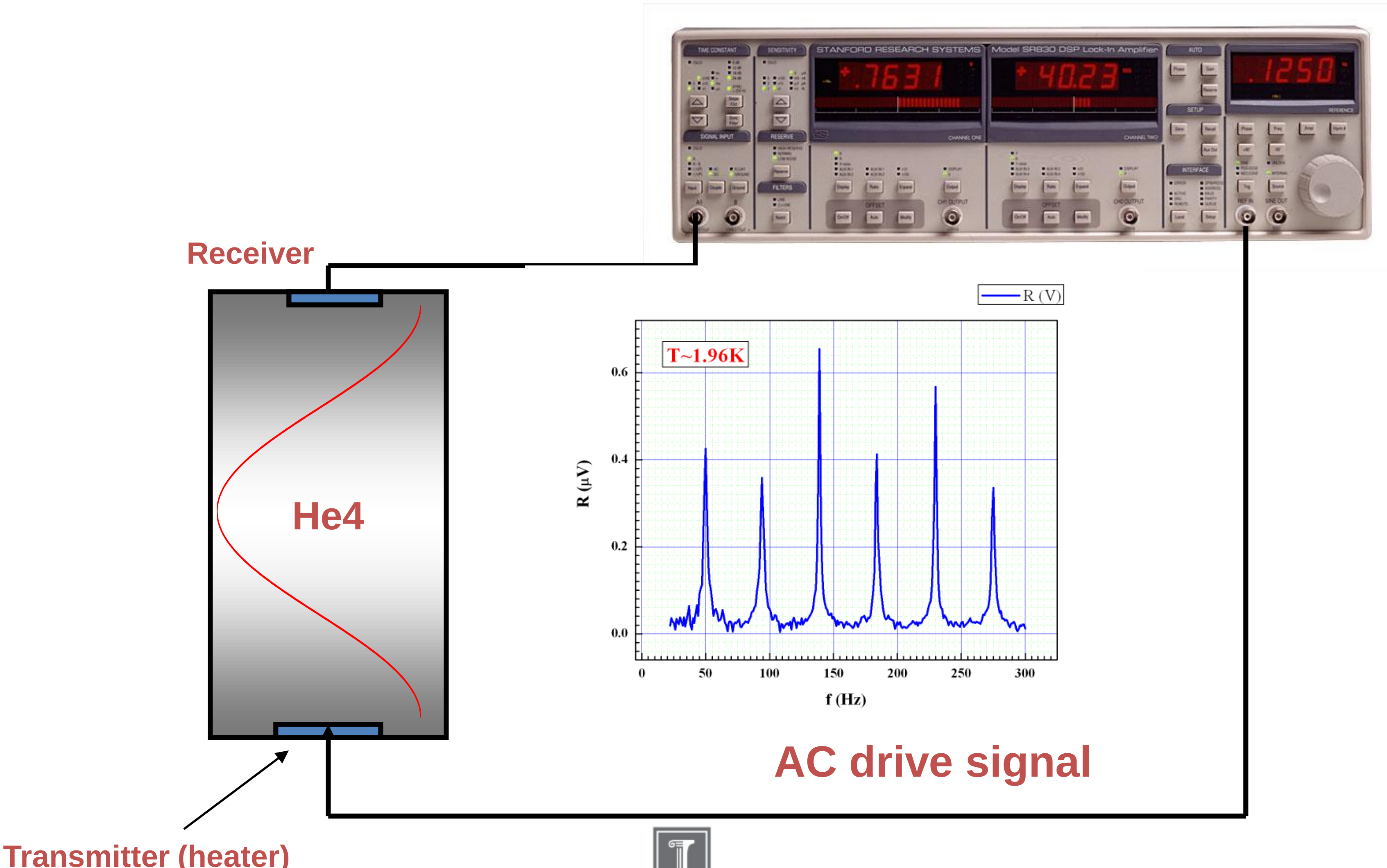


Frequency domain representation of the system

Response function → $\breve{H}(\omega) = \dfrac{\breve{V}_{out}}{\breve{V}_{in}}$

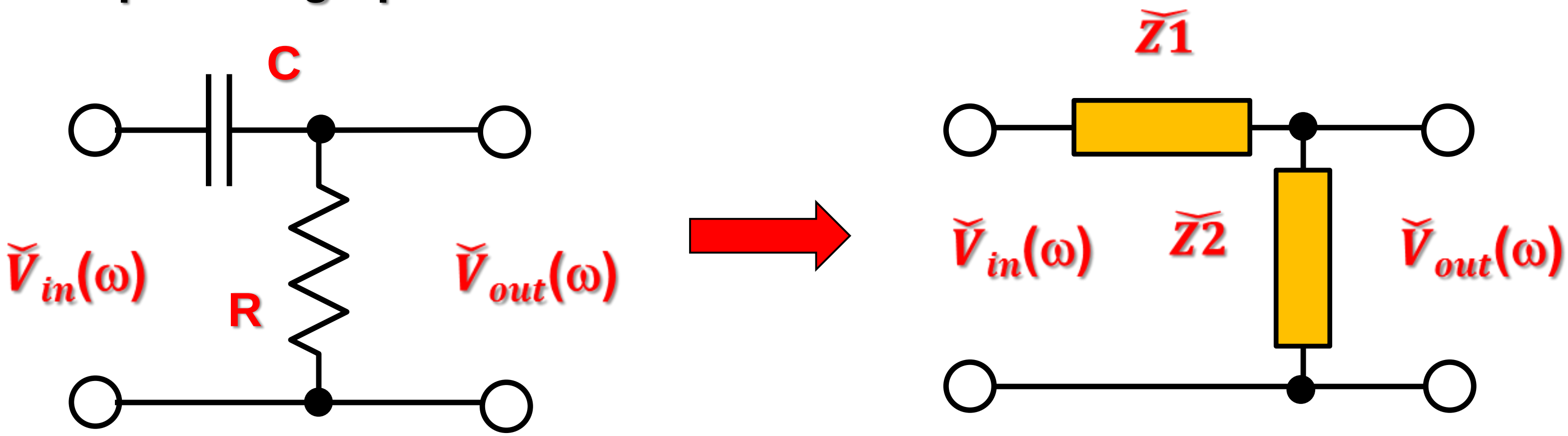
Linear systems are those that can be modeled by linear differential equations.

Typical application of the lock-in amplifier



Experiments. Main idea.
Calculation of the response function in frequency domain mode.

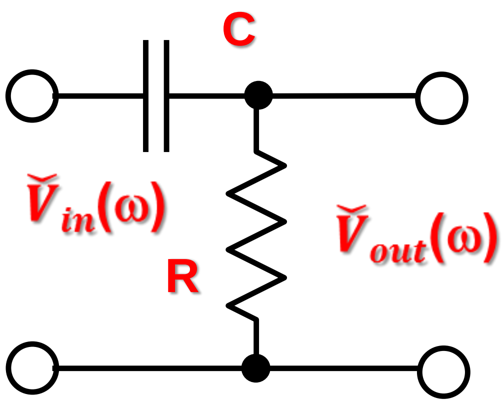
Example 1. High-pass filter.



Applying the Kirchhoff Law to this simple network

$$\tilde{V}_{out}(\omega) = \tilde{H}(\omega) * \tilde{V}_{in}(\omega) = \tilde{V}_{in}(\omega)\frac{\tilde{Z}2(\omega)}{\tilde{Z}1(\omega) + \tilde{Z}2(\omega)}$$

Experiments. Calculation of the response function in frequency domain mode. High-pass filter



Ideal case

$$\tilde{Z}_R = R$$

$$\tilde{Z}_L = j\omega L$$

$$\tilde{Z}_C = \frac{1}{j\omega C} = -\frac{j}{\omega C}$$

More realistic

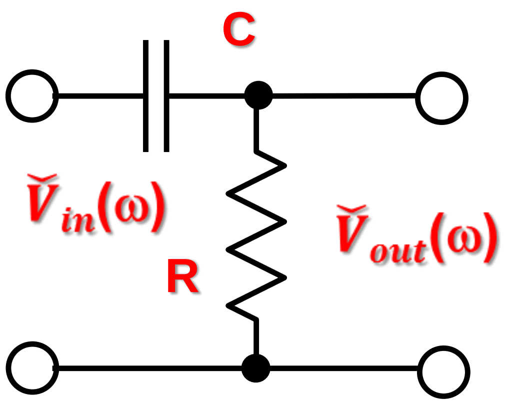
$$\tilde{Z}_R = R + \ldots$$

$$\tilde{Z}_L = j\omega L + R_L$$

$$\tilde{Z}_C = \frac{1}{j\omega C} = \frac{1}{j\omega C + R_C^{-1}}$$

$$\tilde{V}_{out}(\omega) = \tilde{H}(\omega) * \tilde{V}_{in}(\omega) = \tilde{V}_{in}(\omega)\frac{\tilde{Z}2(\omega)}{\tilde{Z}1(\omega) + \tilde{Z}2(\omega)}$$

Experiments. Calculation of the response function in frequency domain mode. High-pass filter



τ – time constant of the filter

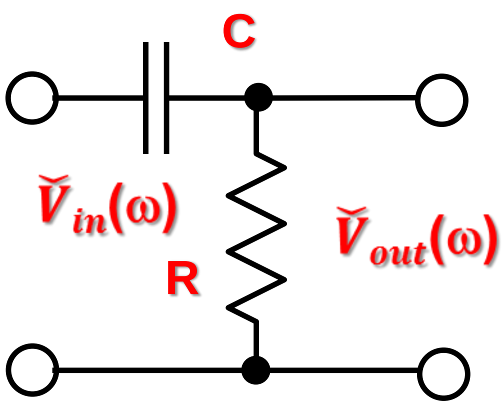
ω_C - cutoff frequency

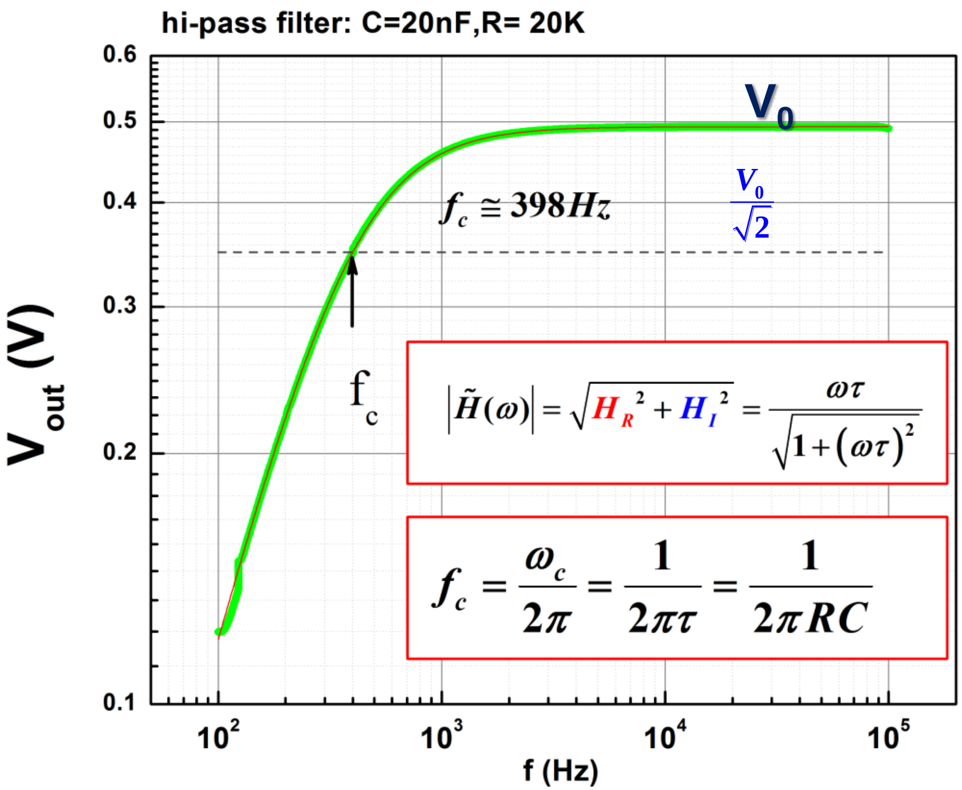
$$\tilde{H}(\omega) = H_R(\omega) + jH_I(\omega) = \frac{R}{R + \frac{1}{j\omega C}} = \frac{j\omega RC}{1 + j\omega RC} = \frac{j\omega\tau}{1 + j\omega\tau} = \frac{\omega\tau}{\left(1+\omega^2\tau^2\right)}\left(\omega\tau + j\right);$$

where $\tau = RC = \omega_c^{-1}$;

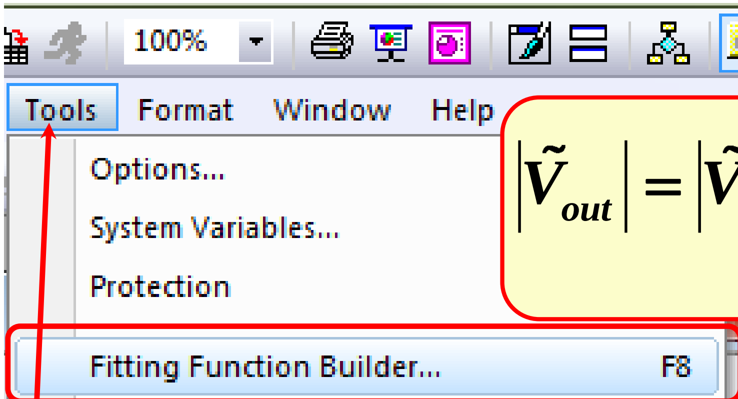
$$\left|\tilde{H}(\omega)\right| = \sqrt{H_R^{\ 2} + H_I^{\ 2}} = \frac{\omega\tau}{\sqrt{1+(\omega\tau)^2}}; \quad \theta(\omega) = \arctan\left(\frac{H_I(\omega)}{H_R(\omega)}\right) = \arctan\left(\frac{1}{\omega\tau}\right)$$

Experiments. Calculation of the response function in frequency domain mode. High-pass filter





High-pass filter. Fitting



$$\left|\tilde{V}_{out}\right| = \left|\tilde{V}_{in}\right| * \left|\tilde{H}(\omega)\right| = V_0 * \frac{\omega\tau}{\sqrt{1+(\omega\tau)^2}}; \quad \tau = RC$$

Fitting parameters: V_0, τ, Voff

Parameters: V0,tau,Voff

Parameters | Constants

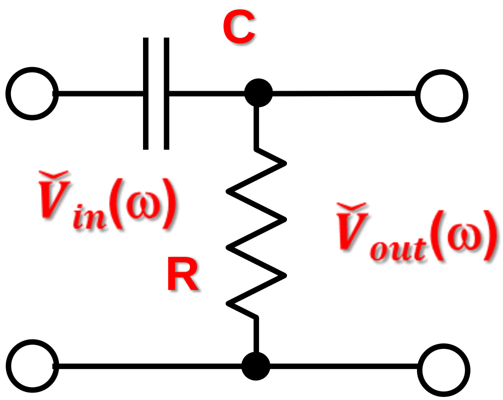
Param	Unit	Meaning	Fixed	Initial Value	Significant Digits
V0		?	☐	1	System
tau		?	☐	1	System
Voff		?	☐	1	System

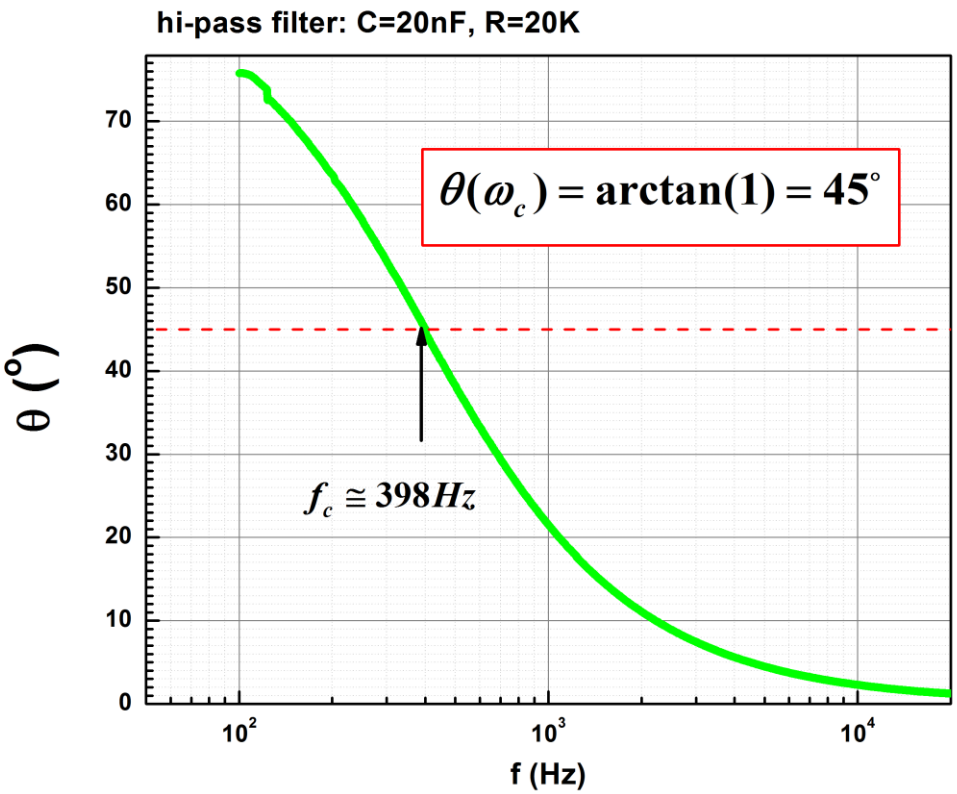
Fitting function →

Function Body (Dependent Variables : y)

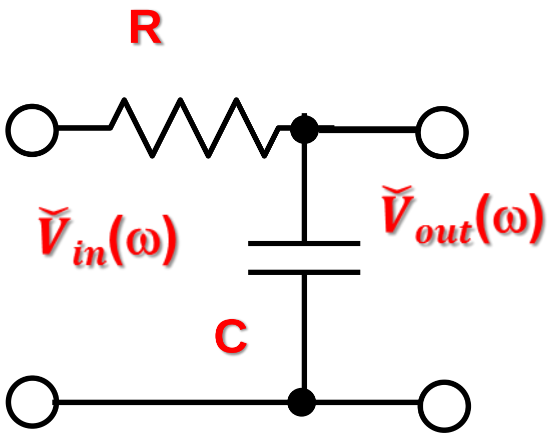
```
y=V0*2*pi*x*tau/sqrt(1+(2*pi*tau)^2)+Voff
```

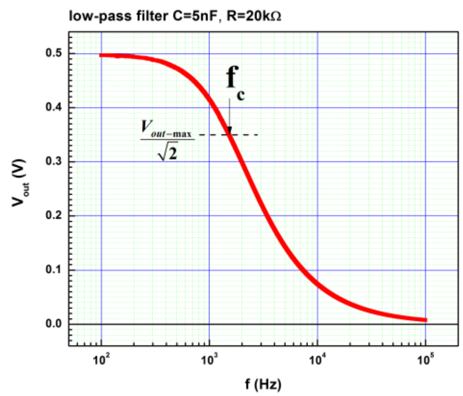
Experiments. Calculation of the response function in frequency domain mode. High-pass filter

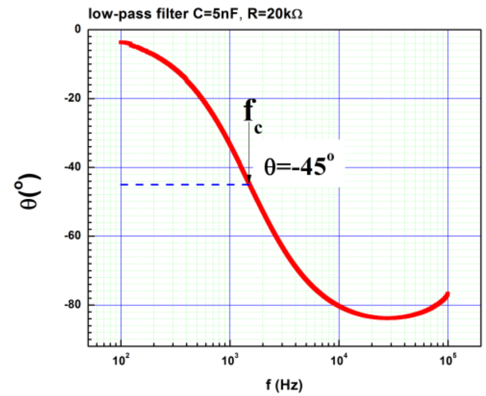




Experiments. Calculation of the response function in frequency domain mode. Low-pass filter





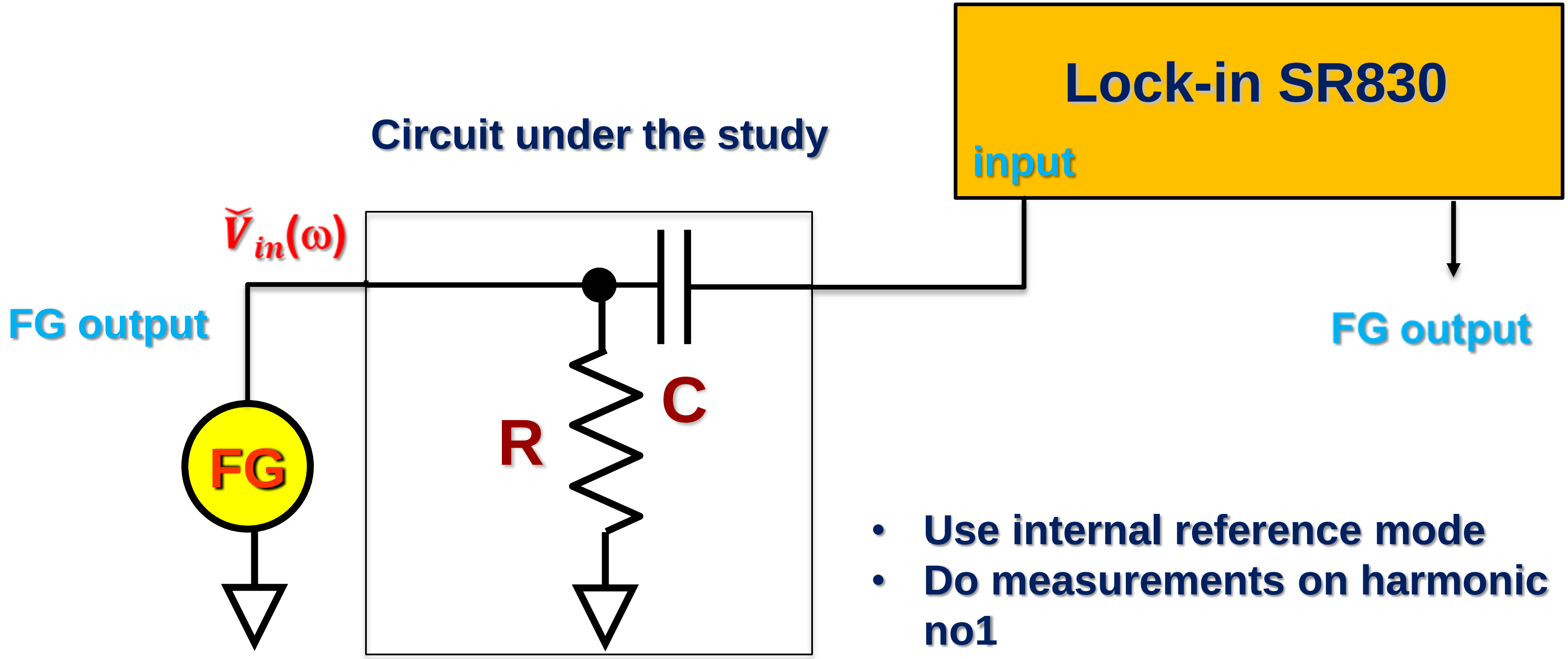


$$\tilde{H}(\omega) = H_R(\omega) + jH_I(\omega) = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{1 + j\omega RC} = \frac{1}{1 + j\omega\tau} = \frac{(1 - j\omega\tau)}{(1 + \omega^2\tau^2)};$$

where $\tau = RC = \omega_c^{-1}$;

$$\left|\tilde{H}(\omega)\right| = \sqrt{H_R^{\ 2} + H_I^{\ 2}} = \frac{1}{\sqrt{1 + (\omega\tau)^2}}; \quad \theta(\omega) = \arctan\left(\frac{H_I(\omega)}{H_R(\omega)}\right) = -\arctan(\omega\tau)$$

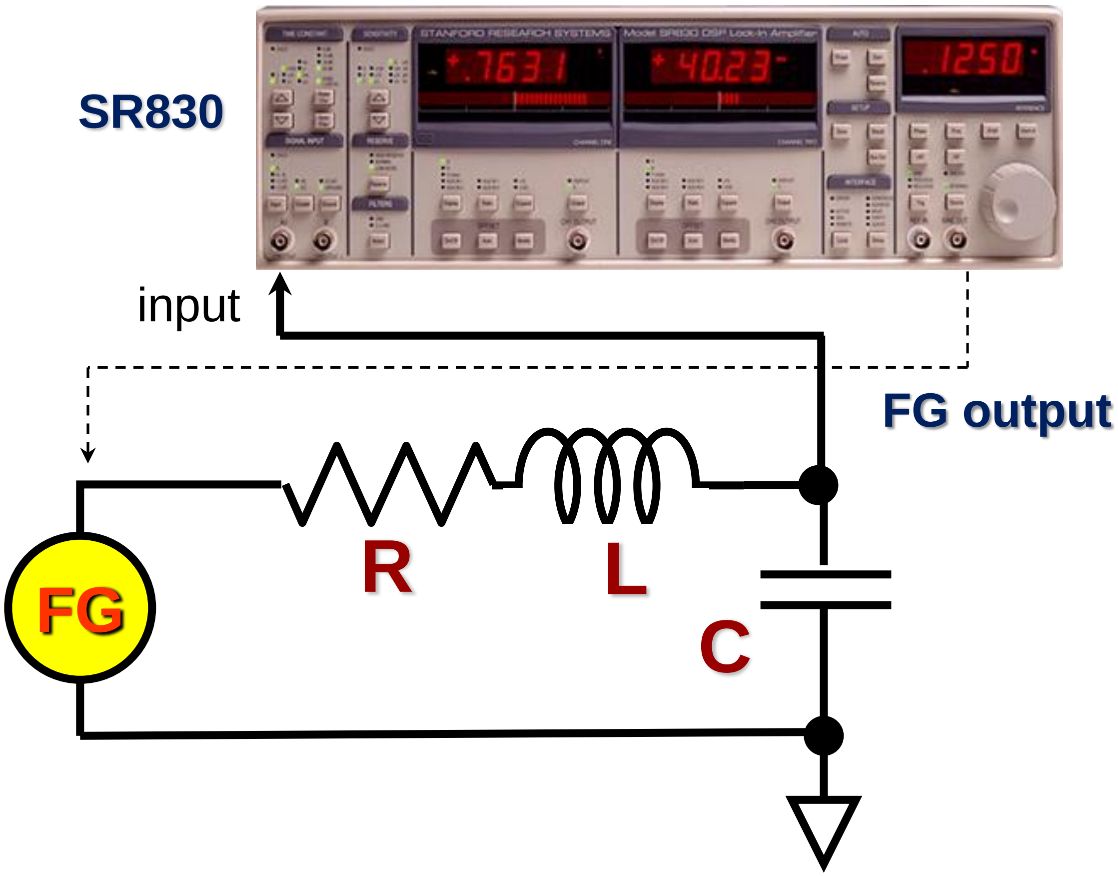
Application of the lock-in amplifier for study of the transfer function of the RLC circuit



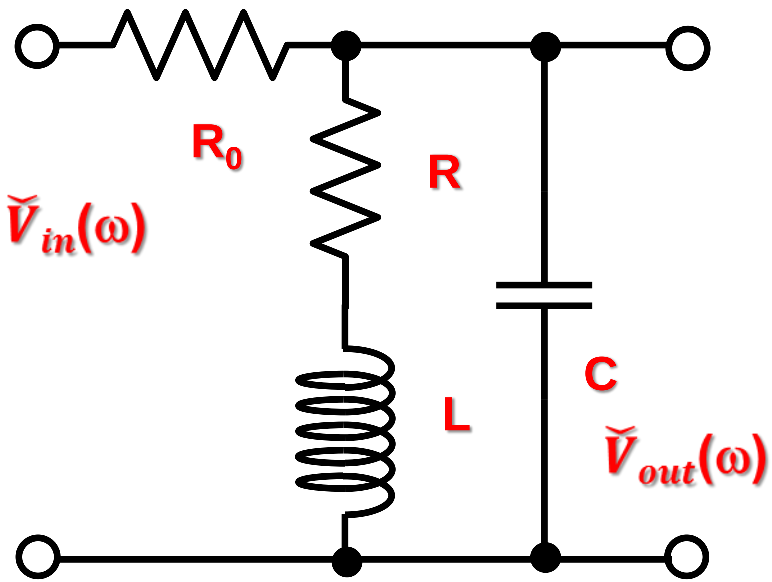
Setup for measuring of the response function of the Hi-pass filter

- Use internal reference mode
- Do measurements on harmonic no1
- Take care about time constant – should be at least ~10 times larger than period of measuring frequency
- Avoid overloading of the lock-in

Setup for measurement of the transfer function of the RLC circuit.



Application of the lock-in amplifier for study of the transfer function of the RLC circuit



$$\tilde{H} = \left(\frac{1}{R_0}\right)\frac{R + j\omega L}{1 - \omega^2 LC + j\omega RC} =$$

$$\left(\frac{1}{R_0}\right)\frac{R + j\omega L}{\left(1 - \frac{\omega^2}{\omega_0^2}\right) + j\omega RC}$$

$$R_0 >> \left| Z_{RLC} \right|$$

$$\omega_o = 2\pi f = \frac{1}{\sqrt{LC}}; \quad Q = \frac{1}{\omega_0 RC} = \frac{1}{R}\sqrt{\frac{L}{C}}$$

Application of the lock-in amplifier for study of the transfer function of the RLC circuit

$$\tilde{H} = \left(\frac{1}{R_0}\right)\frac{R + j\omega L}{\left(1 - \frac{\omega^2}{\omega_0^2}\right) + j\omega RC} = \left(\frac{R}{R_0}\right)\frac{1 + j\frac{\omega}{\omega_0}Q}{\left(1 - \frac{\omega^2}{\omega_0^2}\right) + j\frac{\omega}{\omega_0}\frac{1}{Q}}$$

$$= \left(\frac{R}{R_0}\right)\frac{1 - j\frac{\omega}{\omega_0}\left(\frac{1}{Q} - Q\left(1 - \frac{\omega^2}{\omega_0^2}\right)\right)}{\left(1 - \frac{\omega^2}{\omega_0^2}\right)^2 + \left(\frac{\omega}{\omega_0}\right)^2\frac{1}{Q^2}}$$

$$\omega_o = 2\pi f = \frac{1}{\sqrt{LC}}; \qquad Q = \frac{1}{\omega_0 RC} = \frac{1}{R}\sqrt{\frac{L}{C}}$$

Another style of the transfer function expressions

$$V_{out} = \frac{\omega_0^2 L}{R_0} \times \frac{\delta\omega_0^2 + j\omega\left(\omega_0^2 - \omega^2 - \omega\delta\right)}{\left(\omega_0^2 - \omega^2\right)^2 + \omega^2\delta^2};$$

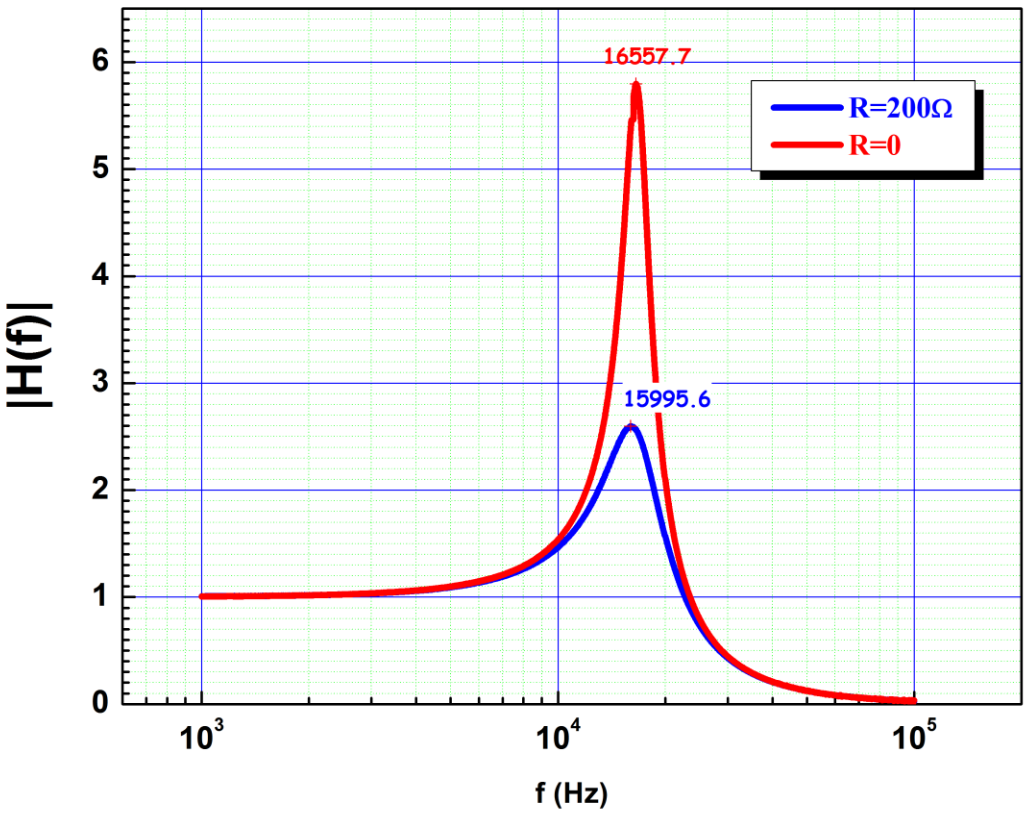
$$X_{out} = \frac{\omega_0^2 L}{R_0} \times \frac{\delta\omega_0^2}{\left(\omega_0^2 - \omega^2\right)^2 + \omega^2\delta^2};$$

$$Y_{out} = \frac{\omega_0^2 L}{R_0} \times \frac{j\omega\left(\omega_0^2 - \omega^2 - \omega\delta\right)}{\left(\omega_0^2 - \omega^2\right)^2 + \omega^2\delta^2};$$

$$\omega_0 = \frac{1}{\sqrt{LC}}; \quad \delta = \frac{R}{L}; \quad Q = \frac{\omega_0}{\delta}$$

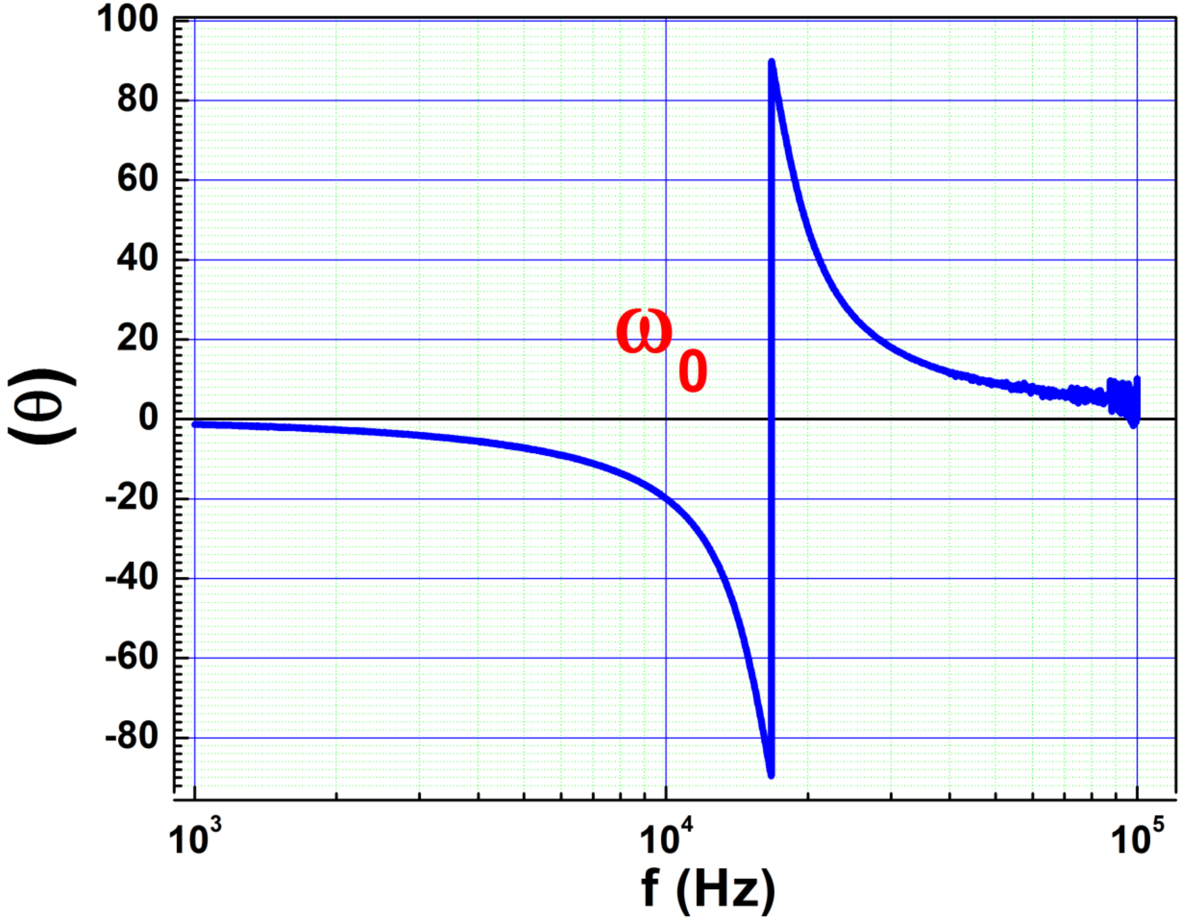
Fitting parameters: $\frac{\omega_0^2 L}{R_0}$ - scaling coefficient ω_0 and δ

Application of the lock-in amplifier for study of the transfer function of the RLC circuit



The resonance curves obtained on RLC circuits with two different damping resistors

Application of the lock-in amplifier for study of the transfer function of the RLC circuit

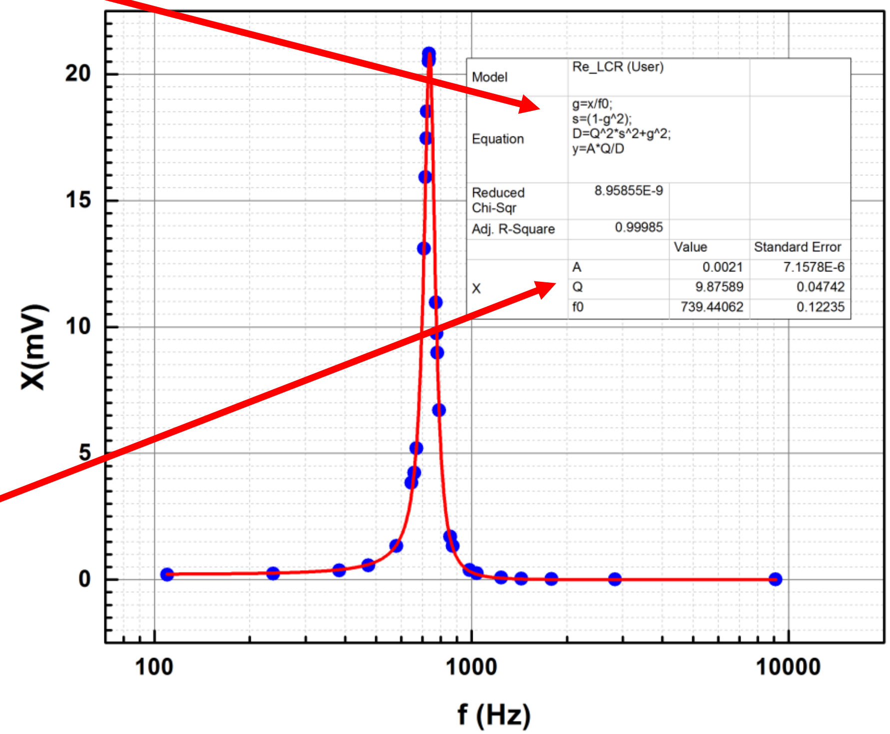


The example of fitting of the RLC circuit date to the analytical expression could be found in:

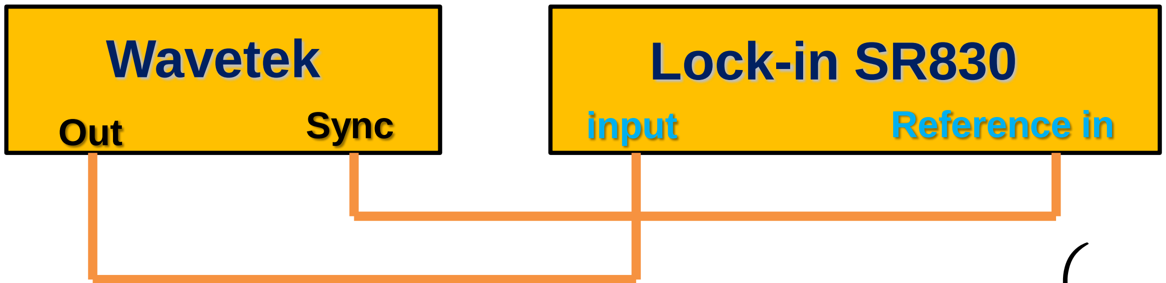
\\engr-file-03\PHYINST\APL Courses\PHYCS401\Common\Simple Examples\Lab 3 Frequency Domain Analysis_example.opjj\

Fitting function

Fitting parameters



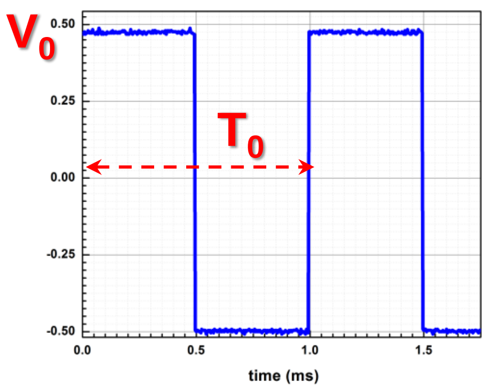
From time domain to frequency domain. Experiment.



F(t) – periodic function $F(t)=F(t+T_0)$:

$$V = V_0 \left(0 < t \le \frac{T_0}{2}\right);$$

$$-V_0 \left(\frac{T_0}{2} < t \le T_0\right)$$



Time domain pattern

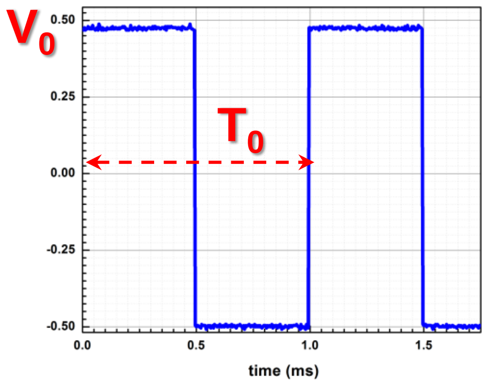
Frequency domain ?

$$a_n = \frac{2}{T_0}\int_0^{T_0} F(t)\cos\left(\frac{2\pi n t}{T_0}\right)dt;$$

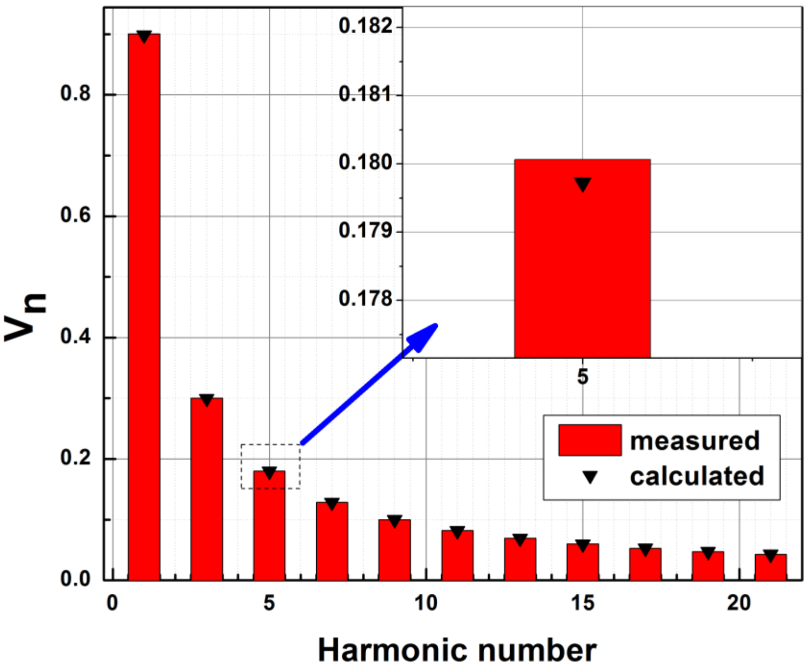
$$b_n = \frac{2}{T_0}\int_0^{T_0} F(t)\sin\left(\frac{2\pi n t}{T_0}\right)dt;$$

$$a_0 = \frac{2}{T_0}\int_0^{T_0} F(t)dt$$

From time domain to frequency domain. Experiment with SR830. Results.



Time domain

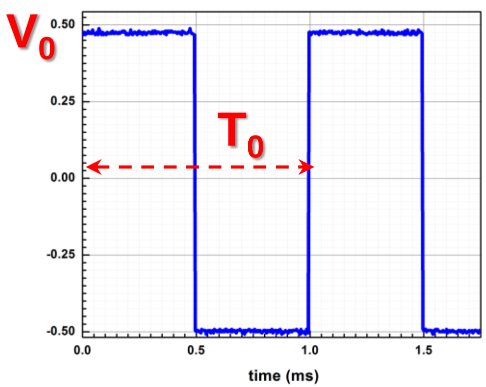


Spectrum measured by SR 830 lock-in amplifier

Time domain pattern

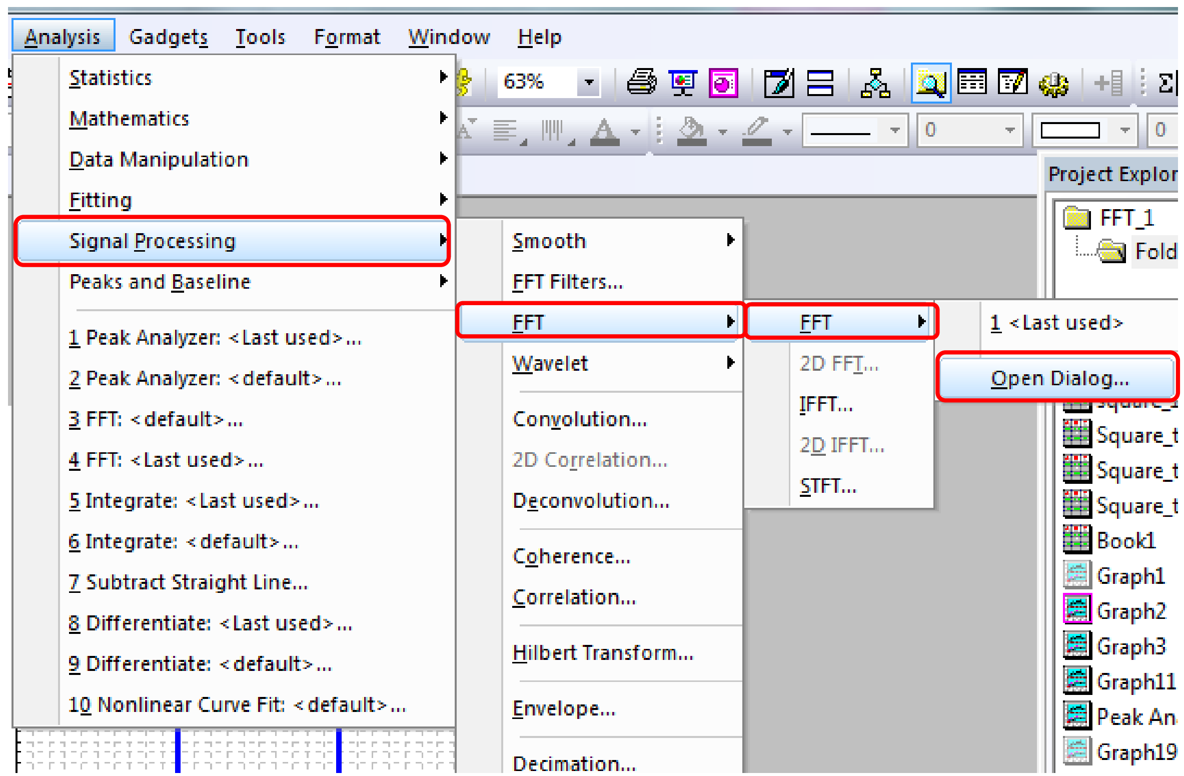
Frequency domain

From time domain to frequency domain. FFT using Origin. Results.

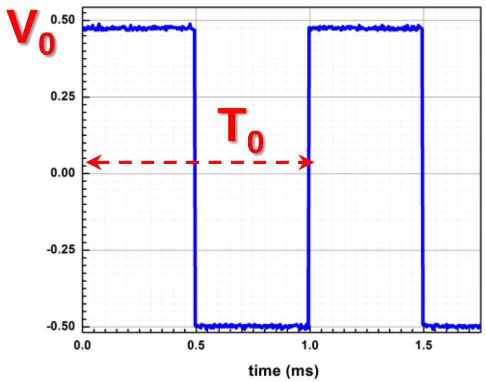


Time domain taken by Tektronix scope

Data file can be used to convert time domain to frequency domain



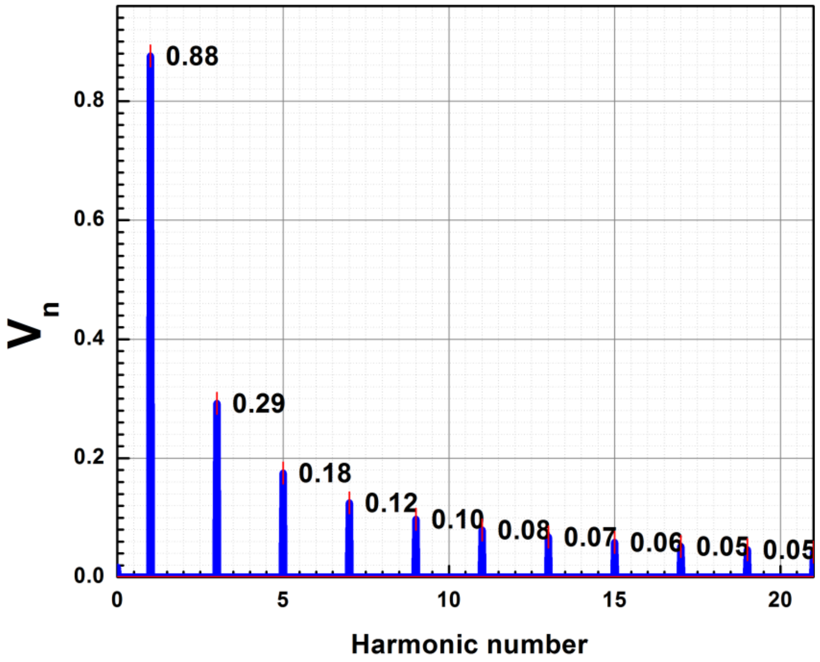
From time domain to frequency domain. FFT using Origin. Results.



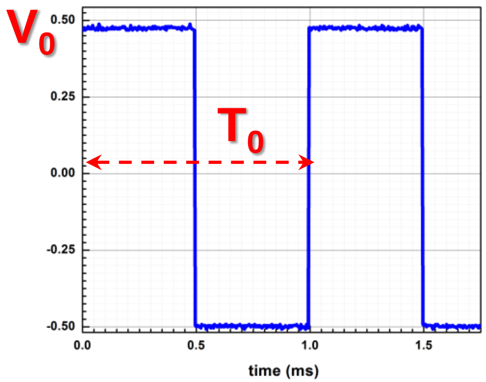
Time domain taken by Tektronix scope

Data file can be used to convert time domain to frequency domain

Spectrum calculated by Origin.
Accuracy is limited because of the limited resolution of the scope

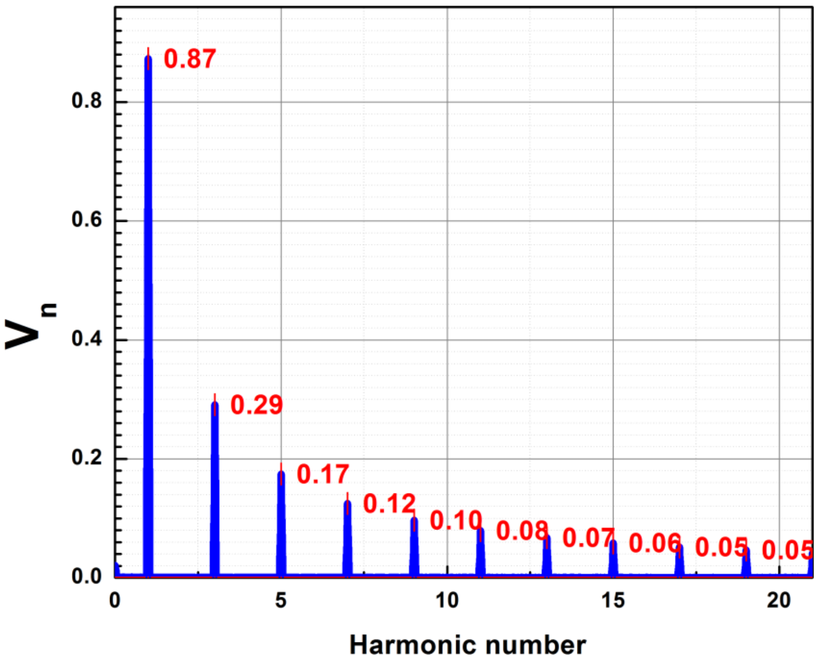


From time domain to frequency domain. Using of the Math option of the scope.



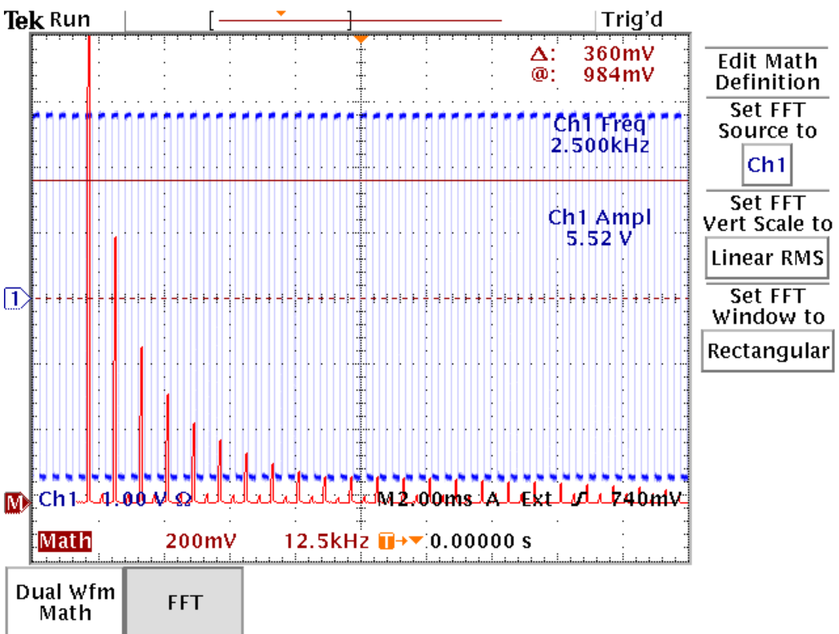
Time domain taken by Tektronix scope

Spectrum calculated by Tektronix scope.

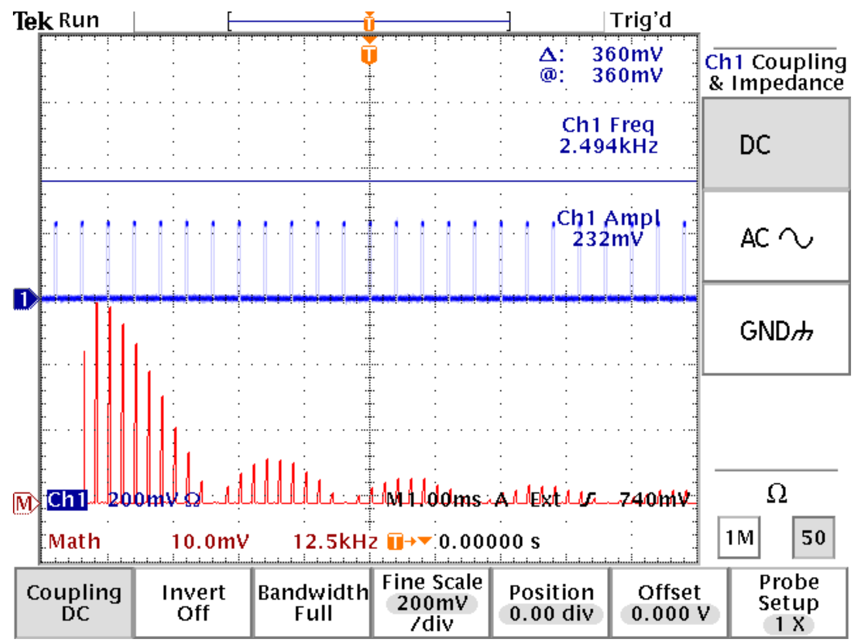


Accuracy is limited because of the limited resolution of the scope

From time domain to frequency domain.
Using of the Math option of the scope.

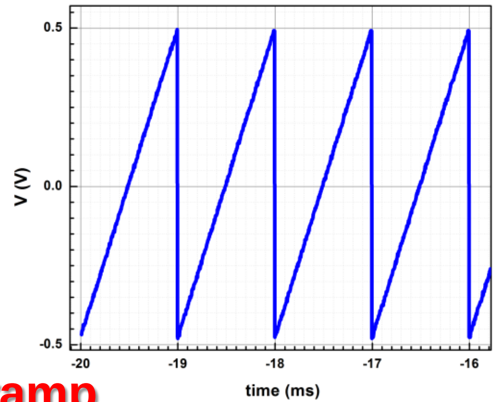


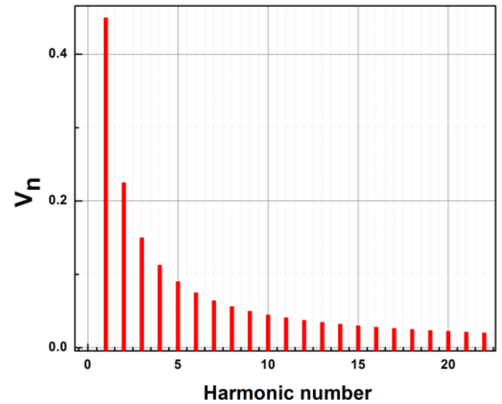
Spectrum of the square wave signal



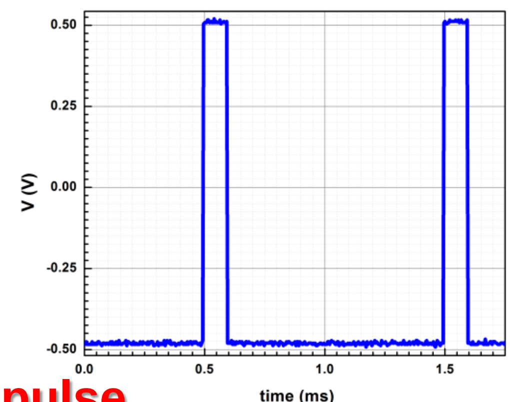
Spectrum of the pulse signal

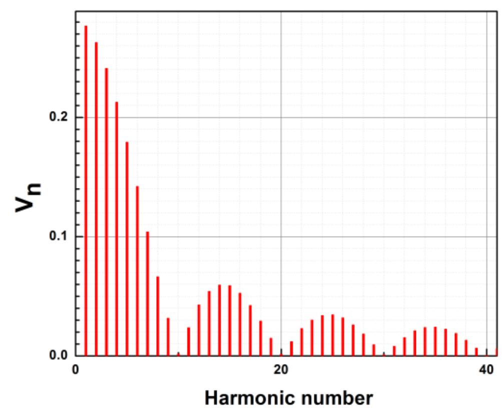
From time domain to frequency domain. Different waveforms. Lock-in.





ramp





pulse

Appendix #1

Reminder: please submit the reports by e-mail in MsWord or pdf format. Strongly recommend the file name structure as:

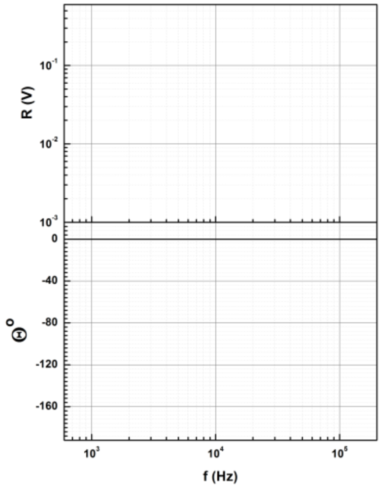
L1_lab2_student1

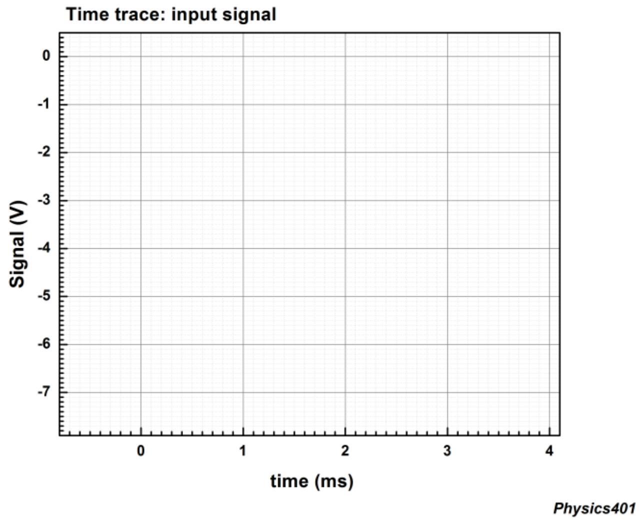
Lab section (L1) — **Lab number** (lab2) — **Your name** (student1)

Appendix #2

Origin templates for the Lab are available in:

\\engr-file-03\PHYINST\APL Courses\PHYCS401\Common\Origin templates\frequency domain analysis





Appendix #3

Lab Server access

\\engr-file-03\PHYINST\APL Courses\PHYCS401

http://it.engineering.illinois.edu/user-guides/remote-access/how-do-i-connect-network-drive-or-file-share

If still there are questions – send the question to the help desk: ***engrit-help@illinois.edu***

References:

1. John H. Scofield, "A Frequency-Domain Description of a Lock-in Amplifier" *American Journal of Physics* 62 (2) 129-133 (Feb. 1994).
2. *Steve Smith* "The Scientist and Engineer's Guide to Digital Signal Processing*" copyright ©1997-1998 by Steven W. Smith. For more information visit the book's website at: www.DSPguide.com" **

- You can find a soft copy of this book in:
- *\\engr-file-03\phyinst\APL Courses\PHYCS401\Experiments*