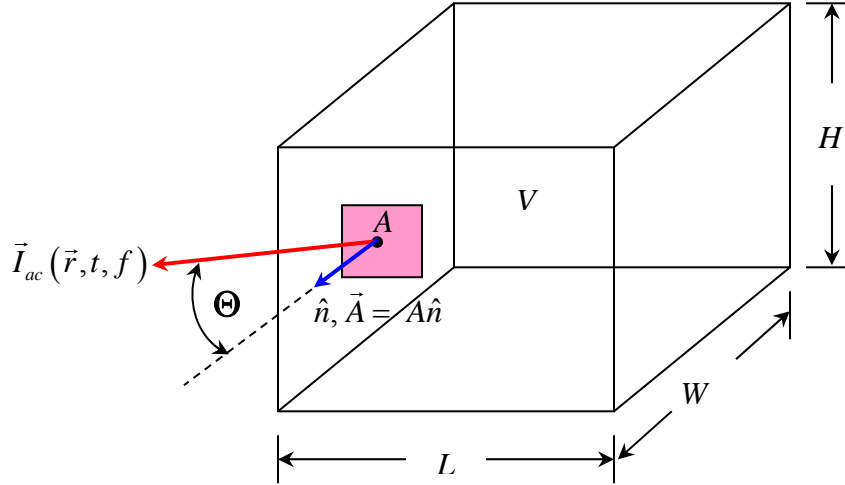


Derivation of the Sabine Equation: Conservation of Energy

Consider a large room of volume $V = H \times W \times L$ (m^3) with perfectly reflecting walls, filled with a uniform, steady-state (*i.e.* equilibrium) acoustic energy density $w_a(\vec{r}, t, f)$ at given frequency f (Hz) within the volume V of the room. Uniform energy density means that a given time t : $w_a(\vec{r}, t, f) = w_a(t, f) = \text{constant}$ (*SI units: Joules/m³*). The large room also has a small opening of area A (m^2) in it, as shown in the figure below:



In the steady-state, the rate of acoustical energy W_a input *e.g.* by a point sound source within the large room equals the rate at which acoustical energy is “leaking” out of the room through the hole of area A , *i.e.* the acoustical power input by the sound source in the room into the room = the acoustical power leaving the room through the hole of area A . In this idealized model of a room with perfectly reflecting walls, the hole of area A thus represents absorption of sound in a real room with finite reflectivity walls, *i.e.* walls that have some absorption associated with them.

Suppose at time $t = 0$ the sound source in the room {located far from the hole} is turned off. Since the sound energy density is uniform in the room, the sound energy contained in the room $W_a(t, f) = \int_V w_a(\vec{r}, t, f) d^3r = w_a(t, f) \int_V d^3r = w_a(t, f)V$ will thus decrease with time, since acoustical energy is (slowly) leaking out of the room through the opening of area A .

The instantaneous acoustical power at the frequency f passing through the hole of area A is the instantaneous time-rate of change of the acoustic energy in the room:

$$P_a(t, f) = \frac{\partial W_a(t, f)}{\partial t}$$

However, the instantaneous acoustical power loss at the frequency f associated with the flux of acoustic energy passing through the hole of area A is also $P_a(t, f) = -\int_A \vec{I}_a(\vec{r}, t, f) \cdot d\vec{A}$ where $\vec{I}_a(\vec{r}, t, f)$ is the instantaneous 3-D vector sound intensity at the point \vec{r} at frequency f (*SI units: Watts/m²*) and $d\vec{A} = dA\hat{n}$ is a infinitesimal vector area element associated with the hole of area A , and \hat{n} is the outward-pointing unit normal to the hole of area A , as shown in the above figure.

Thus:

$$P_a(t, f) = \frac{\partial W_a(t, f)}{\partial t} = -\int_A \vec{I}_a(\vec{r}, t, f) \cdot d\vec{A} = -\int_A \vec{I}_a(\vec{r}, t, f) \cdot \hat{n} dA = -\int_A |I_a(t, f)| \cos \Theta(t) dA$$

where $\cos \Theta(t)$ is the instantaneous direction cosine, and thus $\Theta(t)$ is the instantaneous 3-D opening angle between the two vectors $\vec{I}_a(t, f)$ and $\vec{A} = A\hat{n}$ (as shown in the above figure), and $\vec{I}_a(\vec{r}, t, f) \cdot \hat{n} = |I_a(\vec{r}, f)| \cos \Theta(t)$. In the steady-state, the magnitude of the 3-D vector sound intensity is constant in time at any given point \vec{r} inside the volume V of the room, and on/at the opening of the hole of area A , however the direction of the 3-D vector sound intensity at any given point \vec{r} fluctuates randomly from one moment to the next. At/on the surface of the opening of the hole of area A , the direction of the 3-D vector sound intensity associated with energy leaking out of the room of volume V is such that the direction of the 3-D sound intensity points randomly from moment-to-moment in the forward-going hemisphere, *i.e.* is contained within a solid angle $d\Omega$ associated only with the forward half of 4π steradians (since sound energy is leaking out of the room – sound energy is not coming into the room from the outside).

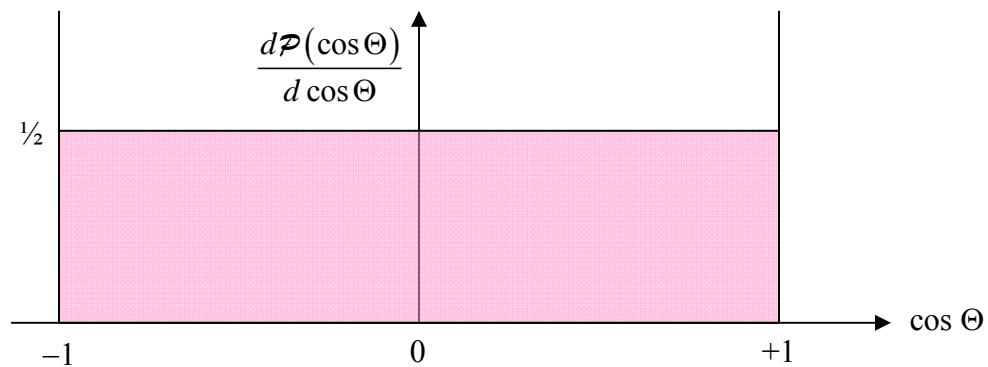
We are not interested in following the instantaneous, moment-to-moment/short-time scale fluctuations in the 3-D vector sound intensity $\vec{I}_a(\vec{r}, t, f)$, but we are interested in the mean power loss, time-averaged over these moment-to-moment fluctuations. For randomly fluctuating direction in $\vec{I}_a(\vec{r}, t, f)$, the mean power loss through the hole of area A , time-averaging over such moment-to-moment fluctuations is:

$$\langle P_a(t, f) \rangle = \frac{\partial \langle W_a(t, f) \rangle}{\partial t} = -\left\langle \int_A \vec{I}_a(\vec{r}_{hole}, t, f) \cdot d\vec{A} \right\rangle = -\int_A |I_a(\vec{r}_{hole}, f)| \langle \cos \Theta(t) \rangle dA$$

The random, fluctuating moment-to-moment direction in the 3-D vector sound intensity $\vec{I}_a(\vec{r}_{hole}, t, f) = \underbrace{|I_a(\vec{r}_{hole}, f)|}_{= \text{constant}} \cos \Theta(t)$ means that the fluctuating, moment-to-moment $\cos \Theta(t)$ is

random at the hole opening of area A . What this means physically is that the probability density distribution $d\mathcal{P}(\cos \Theta)/d \cos \Theta = 1/2$ is flat/uniform in the $\cos \Theta$ variable, as shown in the figure below:

Figure



Since probability \mathcal{P} is (always) conserved, and defining $x \equiv \cos \Theta$, we must have:

$$\int_{-1}^{+1} \left(\frac{d\mathcal{P}(\cos \Theta)}{d \cos \Theta} \right) d \cos \Theta = \int_{-1}^{+1} \left(\frac{d\mathcal{P}(x)}{dx} \right) dx = \int_{-1}^{+1} \frac{1}{2} dx = \frac{1}{2} \int_{-1}^{+1} dx = \frac{1}{2} x \Big|_{-1}^{+1} = \frac{1}{2} \cdot 2 = 1$$

However, for our physical situation *here*, only the forward half of this probability distribution is occupied ($0 \leq \cos \Theta \leq 1$) - {sound energy is leaking out of the hole, not into it}. Thus, the time-averaged value of $\cos \Theta(t)$, for a flat random distribution in $\cos \Theta$ over the forward hemisphere is:

$$\langle \cos \Theta(t) \rangle = \int_0^1 \left(\frac{d\mathcal{P}(\cos \Theta)}{d \cos \Theta} \right) \cos \Theta d \cos \Theta = \int_0^1 \left(\frac{1}{2} \right) \cos \Theta d \cos \Theta = \frac{1}{2} \int_0^1 x dx = \frac{1}{2} \cdot \frac{1}{2} x^2 \Big|_0^1 = \frac{1}{4}$$

and hence:

$$\begin{aligned} \langle P_a(t, f) \rangle &= \frac{\partial \langle W_a(t, f) \rangle}{\partial t} = - \left\langle \int_A \vec{I}_a(\vec{r}, t, f) \cdot d\vec{A} \right\rangle = - \int_A |I_a(\vec{r}, f)| \langle \cos \Theta(t) \rangle dA \\ &= - \frac{1}{4} \int_A |I_a(\vec{r}, f)| dA = - \frac{1}{4} |I_a(\vec{r}_{hole}, f)| \int_A dA = - \frac{1}{4} |I_a(\vec{r}_{hole}, f)| A \end{aligned}$$

A clarificational note: In the steady-state, note that the time interval Δt_{avg} needed for averaging over the moment-to-moment fluctuations in the instantaneous direction of the 3-D sound intensity $\vec{I}_a(\vec{r}, t, f)$ is much less than the characteristic time constant τ_w associated with sound energy leaking out of the room of volume V through the hole of area A , *i.e.* $\Delta t_{avg} \ll \tau_w$.

For a large room, we {can safely} assume that the nature of sound propagation is very similar to that in “free air” – *i.e.* the great outdoors. Then the instantaneous 3-D vector sound intensity $\vec{I}_a(\vec{r}, t, f)$ is related to the instantaneous scalar acoustic energy density $w_a(\vec{r}, t, f)$ (*Joules/m³*) by the relation $\vec{I}_a(\vec{r}, t, f) = \vec{c} w_a(\vec{r}, t, f)$ where \vec{c} = velocity vector associated with propagation of sound in free-air with $|\vec{c}| \approx 344 \text{ m/s}$ at *NTP*. Thus, from the above discussion on averaging out random, moment-to-moment fluctuations in the direction of 3-D sound intensity at the hole of area A , we see that the time-averaged version of this relation also holds:

$$\langle \vec{I}_a(\vec{r}, t, f) \rangle = \langle \vec{c} w_a(\vec{r}, t, f) \rangle \Rightarrow \langle I_a(\vec{r}_{hole}, t, f) \rangle = c \langle w_a(\vec{r}_{hole}, t, f) \rangle$$

Note further that in the steady-state, at time t the acoustic energy $W_a(t, f)$ contained within the room of volume V is related to the {uniform} acoustic energy density $w_a(\vec{r}, t, f)$ by:

$$W_a(t, f) = \int_V w_a(\vec{r}, t, f) d^3 r = w_a(t, f) \int_V d^3 r = w_a(t, f) V$$

This relation also holds for time-averaged quantities:

$$\langle W_a(t, f) \rangle = \int_V \langle w_a(\vec{r}, t, f) \rangle d^3 r = \langle w_a(t, f) \rangle \int_V d^3 r = \langle w_a(t, f) \rangle V$$

Since the acoustic energy leaking out of the hole comes from inside the room, by energy conservation, we see that:

$$\begin{aligned}\langle P_a(t, f) \rangle &= \frac{\partial \langle W_a(t, f) \rangle}{\partial t} = - \left\langle \int_A \vec{I}_a(\vec{r}, t, f) \cdot d\vec{A} \right\rangle = - \frac{1}{4} \langle I_a(\vec{r}_{hole}, t, f) \rangle A = - \frac{1}{4} c \langle w_a(\vec{r}_{hole}, t, f) \rangle A \\ &= - \frac{cA}{4V} \langle W_a(t, f) \rangle\end{aligned}$$

or:

$$\frac{\partial \langle W_a(t, f) \rangle}{\partial t} = - \frac{cA}{4V} \langle W_a(t, f) \rangle = - \frac{1}{\tau_w} \langle W_a(t, f) \rangle$$

where we have defined the characteristic time constant $\tau_w \equiv \frac{4V}{cA}$ (SI units: *seconds*).

The equation $\frac{\partial \langle W_a(t, f) \rangle}{\partial t} = - \frac{1}{\tau_w} \langle W_a(t, f) \rangle$ is a linear, first-order homogeneous differential equation {known as the diffusion, or heat equation} which, for our situation/our initial conditions (at $t = 0$) has the well-known solution of the form:

$$\langle W_a(t, f) \rangle = \langle W_a^o(f) \rangle e^{-t/\tau_w}$$

where $\langle W_a^o(f) \rangle$ is the time-averaged value of the acoustic energy contained in the room at the frequency f at time $t = 0$. Thus, at time $t = \tau_w$: $\langle W_a(f, t = \tau_w) \rangle = \langle W_a^o(f) \rangle e^{-\tau_w/\tau_w} = \langle W_a^o(f) \rangle e^{-1}$ *i.e.* the {time-averaged} acoustic energy at frequency f decreases to $1/e = 1/2.7183 = 0.3679$ of its initial value in a time interval $t = \tau_w$.

For a large room, since $\langle I_a(f, t) \rangle = c \langle w_a(f, t) \rangle = c \langle W_a(f, t) \rangle / V$, we can equivalently rewrite the solution for the time-averaged acoustic energy in terms of the time-averaged sound intensity as: $\langle I_a(t, f) \rangle = \langle I_a^o(f) \rangle e^{-t/\tau_w}$ where $\langle I_a^o(f) \rangle$ is the time-averaged sound intensity at the frequency f at time $t = 0$, and instead ask: how long does it take for the time-averaged sound intensity to decay to one-millionth (10^{-6}) of its initial value, *i.e.* what is the **reverberation time** T_{60} ? This occurs when:

$$\langle I_a(t = T_{60}, f) \rangle = \langle I_a^o(f) \rangle e^{-T_{60}/\tau_w} = 10^{-6} \langle I_a^o(f) \rangle$$

i.e. this occurs when $e^{-T_{60}/\tau_w} = 10^{-6}$. Take the natural log of both sides of this relation:

$$\ln(e^{-T_{60}/\tau_w}) = \ln(10^{-6}). \text{ But } \ln(e^{-T_{60}/\tau_w}) = -T_{60}/\tau_w. \text{ Thus: } -T_{60}/\tau_w = \ln(10^{-6}) \text{ or:}$$

$$T_{60} = -\tau_w \ln(10^{-6}) \text{ and since } \tau_w \equiv \frac{4V}{cA}, \text{ we thus find that the } \mathbf{reverberation time } T_{60} \text{ is:}$$

$$T_{60} = -\tau_w \ln(10^{-6}) = \left\{ \frac{4V}{cA} \right\} \ln(10^{-6}) = \left\{ - \frac{4 \cdot \ln(10^{-6})}{c} \right\} \frac{V}{A} = \kappa \frac{V}{A}$$

The numerical value of this “universal” constant, κ is:

$$\kappa \equiv -\frac{4 \cdot \ln(10^{-6})}{c} = +\frac{4 \cdot 13.8155}{343 \text{ m/s}} = +\frac{55.262}{343 \text{ m/s}} = 0.1611 \text{ s/m} (= 0.049 \text{ s/ft})$$

Thus, the **Sabine equation** is: $T_{60} = 0.161 \frac{V}{A}$ (*metric units*) = $0.049 \frac{V}{A}$ (*english units*).

We also see that: $T_{60} = -\tau_w \ln(10^{-6.0}) = 13.8155 \tau_w$.

Similarly, we can also show that the **reverberation time** T_{30} , defined as the time it takes for the time-averaged sound intensity to decay to one-thousandth (10^{-3}) of its initial value is given by:

$$T_{30} = -\tau_w \ln(10^{-3.0}) = 6.9078 \tau_w = \frac{1}{2} T_{60}$$

How do we physically measure/determine the **reverberation time** T_{60} (and/or T_{30})?

Method I:

Note that since:

$$\begin{aligned} \langle I_a(t = T_{60}, f) \rangle &= \langle I_a^o(f) \rangle e^{-T_{60}/\tau_w} = 10^{-6} \langle I_a^o(f) \rangle \\ \langle I_a(t = T_{30}, f) \rangle &= \langle I_a^o(f) \rangle e^{-T_{30}/\tau_w} = 10^{-3} \langle I_a^o(f) \rangle \end{aligned}$$

Then, from the above {time-averaged} sound intensity level formulae:

$$\begin{aligned} \langle SIL(t = T_{60}, f) \rangle &= 10 \log_{10} \left(\langle I_a(t = T_{60}, f) \rangle / \langle I_o \rangle \right) \\ \langle SIL(t = T_{30}, f) \rangle &= 10 \log_{10} \left(\langle I_a(t = T_{30}, f) \rangle / \langle I_o \rangle \right) \end{aligned}$$

where $\langle I_o \rangle = 10^{-12} \text{ Watts/m}^2$ is the (time-averaged) reference sound intensity (at the threshold of human hearing).

At time $t = 0$ we have:

$$\begin{aligned} \langle SIL(t = 0, f) \rangle &= 10 \log_{10} \left(\langle I_a(t = 0, f) \rangle / \langle I_o \rangle \right) \\ &= 10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right) \end{aligned}$$

Thus, the $t = 0$ to $t = T_{60}$ difference in {time-averaged} sound intensity levels is:

$$\begin{aligned}
 \Delta \langle SIL(\Delta t = T_{60}, f) \rangle &\equiv \langle SIL(t = T_{60}, f) \rangle - \langle SIL(t = 0, f) \rangle \\
 &= 10 \log_{10} \left(\langle I_a(t = T_{60}, f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a(t = 0, f) \rangle / \langle I_o \rangle \right) \\
 &= 10 \log_{10} \left(10^{-6} \langle I_a^o(f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right) \\
 &= 10 \log_{10} (10^{-6}) + \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} - \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} \\
 &= 10 \log_{10} (10^{-6}) = -60 \text{ dB}
 \end{aligned}$$

Likewise, the $t = 0$ to $t = T_{30}$ difference in {time-averaged} sound intensity levels is:

$$\begin{aligned}
 \Delta \langle SIL(\Delta t = T_{30}, f) \rangle &\equiv \langle SIL(t = T_{30}, f) \rangle - \langle SIL(t = 0, f) \rangle \\
 &= 10 \log_{10} \left(\langle I_a(t = T_{30}, f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a(t = 0, f) \rangle / \langle I_o \rangle \right) \\
 &= 10 \log_{10} \left(10^{-3} \langle I_a^o(f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right) \\
 &= 10 \log_{10} (10^{-3}) + \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} - \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} \\
 &= 10 \log_{10} (10^{-3}) = -30 \text{ dB}
 \end{aligned}$$

Now, for a large room (*i.e.* in a “free field” situation), the sound intensity level (*SIL*) will be within $\sim 0.1 \text{ dB}$ of the sound pressure level (*SPL*) over the human auditory range ($\sim 20 \text{ Hz} - 20 \text{ KHz}$). Thus, using an accurately-calibrated *SPL* meter, technically speaking, the **reverberation time** $T_{60} = \Delta t = t_2 - t_1$ is the measured time interval corresponding to a decrease of:

$$\begin{aligned}
 \Delta \langle SPL(\Delta t = T_{60}, f) \rangle &= -60 \text{ dB} \text{ measured from } \Delta \langle SPL(t = t_1, f) \rangle = -5 \text{ dB to} \\
 \Delta \langle SPL(t = t_2, f) \rangle &= -65 \text{ dB} \text{ referenced to } \langle SPL(t = 0, f) \rangle.
 \end{aligned}$$

Similarly, technically speaking, the **reverberation time** $T_{30} = \Delta t = t'_2 - t'_1$ is the measured time interval corresponding to a decrease of:

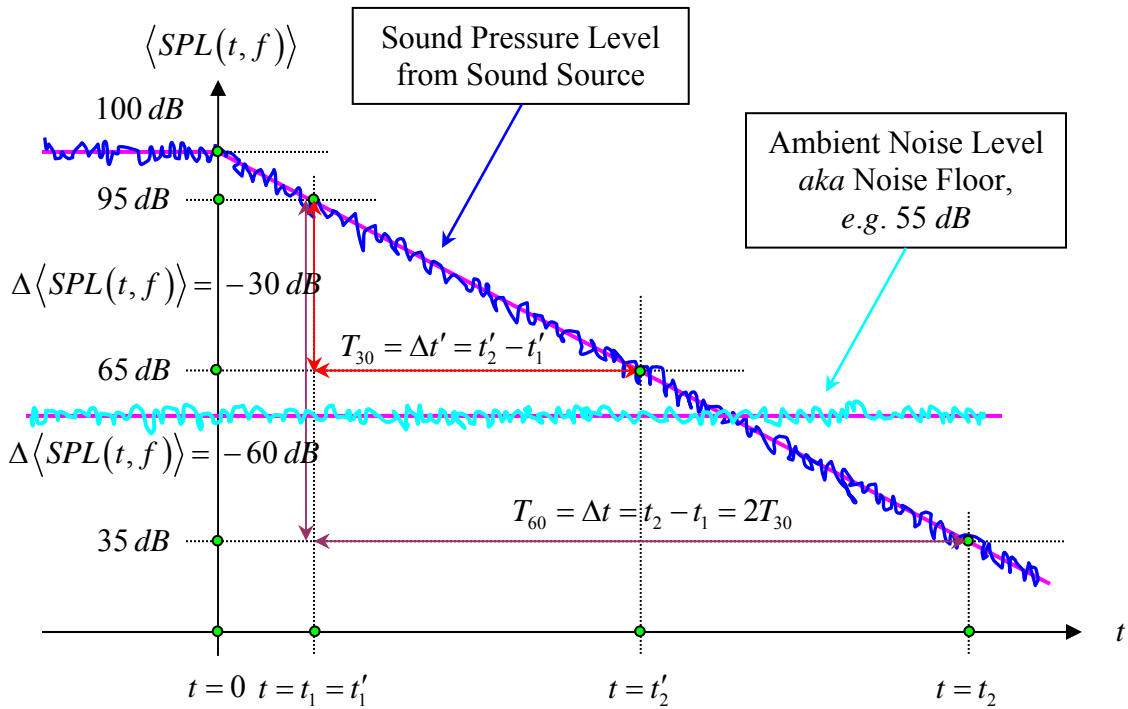
$$\begin{aligned}
 \Delta \langle SPL(\Delta t = T_{30}, f) \rangle &= -30 \text{ dB} \text{ measured from } \Delta \langle SPL(t = t'_1, f) \rangle = -5 \text{ dB to} \\
 \Delta \langle SPL(t = t'_2, f) \rangle &= -35 \text{ dB} \text{ referenced to } \langle SPL(t = 0, f) \rangle.
 \end{aligned}$$

For example, if $\langle SPL(t = 0, f) \rangle = 100 \text{ dB}$, then $\langle SPL(t = t_1, f) \rangle = \langle SPL(t = t'_1, f) \rangle = 95 \text{ dB}$ and $\langle SPL(t = t_2, f) \rangle = 35 \text{ dB}$, whereas $\langle SPL(t = t'_2, f) \rangle = 65 \text{ dB}$, thus:

$$\begin{aligned}
 \Delta \langle SPL(\Delta t = T_{60}, f) \rangle &= \langle SPL(t = t_2, f) \rangle - \langle SPL(t = t_1, f) \rangle = 35 \text{ dB} - 95 \text{ dB} = -60 \text{ dB} \\
 \text{and:} & \\
 \Delta \langle SPL(\Delta t = T_{30}, f) \rangle &= \langle SPL(t = t'_2, f) \rangle - \langle SPL(t = t'_1, f) \rangle = 65 \text{ dB} - 95 \text{ dB} = -30 \text{ dB}
 \end{aligned}$$

$t_1 = t'_1$

These relations are shown in the figure below:



Note that the ambient noise level (*aka* noise floor) of the room may (often) be such that it is significantly above $\langle SPL(t=t_2, f) \rangle = 35 \text{ dB}$ (e.g. 55 dB), hence measuring the T_{60} reverberation time will **not** be possible, whereas measuring the T_{30} reverberation time **will** be possible (as long as the noise floor of the room is below $\langle SPL(t=t'_2, f) \rangle = 65 \text{ dB}$). The T_{60} reverberation time can then be **calculated** from the **measured** T_{30} reverberation time using the simple relation $T_{60} = 2T_{30}$.

Note that one can also simply increase the sound power input to the room, such that with e.g. $\langle SPL(t=0, f) \rangle = 120 \text{ dB}$, then: $\langle SPL(t=t_1, f) \rangle = \langle SPL(t=t'_1, f) \rangle = 115 \text{ dB}$, $\langle SPL(t=t_2, f) \rangle = 55 \text{ dB}$, and $\langle SPL(t=t'_2, f) \rangle = 85 \text{ dB}$, thus:

$$\Delta \langle SPL(\Delta t = T_{60}, f) \rangle = \langle SPL(t=t_2, f) \rangle - \langle SPL(t=t_1, f) \rangle = 55 \text{ dB} - 115 \text{ dB} = -60 \text{ dB}$$

and:

$$\Delta \langle SPL(\Delta t = T_{30}, f) \rangle = \langle SPL(t=t'_2, f) \rangle - \langle SPL(t=t'_1, f) \rangle = 85 \text{ dB} - 115 \text{ dB} = -30 \text{ dB}$$

Note further that there is nothing sacred about using T_{60} or T_{30} ; We can also define other reverberation times: $T_{10}, T_{20}, T_{40}, T_{50}$... which correspond to relative decreases of SIL's/SPL's of $-10, -20, -40, -50$... dB respectively ... The general relation for an arbitrary definition of the reverberation time is: $T_{xx} \equiv -\tau_w \ln(10^{-(xx/10)})$, with: $\Delta \langle SPL(\Delta t = T_{xx}, f) \rangle = -xx \text{ dB}$.

Method II:

Note that since: $\langle I_a(t = \tau_w, f) \rangle = \langle I_a^o(f) \rangle e^{-t/\tau_w} = (1/e) \langle I_a^o(f) \rangle = 0.3679 \langle I_a^o(f) \rangle$

we can use a **true sound intensity meter** (e.g. Bruel & Kjaer 2260E) to measure the time interval $\Delta t = \tau_w - 0 = \tau_w$ that the time-averaged sound intensity falls to $1/e = 0.3679$ of its initial ($t = 0$) value. We can then subsequently calculate T_{60} and T_{30} using the relations:

$$\boxed{T_{60} = -\tau_w \ln(10^{-6.0}) = 13.8155 \tau_w} \quad \text{and:} \quad \boxed{T_{30} = -\tau_w \ln(10^{-3.0}) = 6.9078 \tau_w = \frac{1}{2} T_{60}}$$

However, note that if the typical T_{60} reverberation time is ~ 1.4 sec, then $T_{30} = \frac{1}{2} T_{60} \sim 0.7$ sec and $\tau_w \sim 0.1$ sec! Hence, experimentally it is much better to (directly) measure T_{60} and/or T_{30} if the time resolution of the measurement, $\sigma_t \sim \tau_w \sim 0.1$ sec.

Note further that the following is also a difficult quantity to (accurately) measure:

$$\begin{aligned} \Delta \langle SIL(\Delta t = \tau_w, f) \rangle &\equiv \langle SIL(t = \tau_w, f) \rangle - \langle SIL(t = 0, f) \rangle \approx \Delta \langle SPL(\Delta t = \tau_w, f) \rangle \\ &= 10 \log_{10} \left(\langle I_a(t = \tau_w, f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a(t = 0, f) \rangle / \langle I_o \rangle \right) \\ &= 10 \log_{10} \left((1/e) \langle I_a^o(f) \rangle / \langle I_o \rangle \right) - 10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right) \\ &= 10 \log_{10} (1/e) + \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} - \cancel{10 \log_{10} \left(\langle I_a^o(f) \rangle / \langle I_o \rangle \right)} \\ &= 10 \log_{10} (1/e) = -4.343 \text{ dB} \end{aligned}$$

However, additionally note that one could very easily carry out a least-squares fit of the $SIL(t)$ (or $SPL(t)$) data to a decaying exponential in order to obtain an accurate determination of τ_w .

Method III:

For a large room (i.e. in a “free field” situation), the (time-averaged) sound intensity $\langle I_a(t, f) \rangle$ is related to the time-averaged square of the instantaneous over-pressure by the relation:

$$\langle I_a(t, f) \rangle = \langle p^2(t, f) \rangle / \rho_o c$$

where $\rho_o = 1.204 \text{ kg/m}^3$ is the density of air and $c = 343 \text{ m/s}$ is the longitudinal speed of propagation of sound in air {at NTP}.

Then since: $\langle I_a(t, f) \rangle = \langle I_a^o(f) \rangle e^{-t/\tau_w}$, then: $\langle p^2(t, f) \rangle = \langle p^2(t = 0, f) \rangle e^{-t/\tau_w}$

For a large room (i.e. in a “free field” situation), the time-average square of the over-pressure **amplitude** is related to the over-pressure amplitude by:

$$\langle p^2(t, f) \rangle = \langle p^2(t = 0, f) \rangle e^{-t/\tau_w} = \frac{1}{2} p_o^2 e^{-t/\tau_w}$$

where p_o is the over-pressure amplitude at $t = 0$, and $p(t, f) = p(t = 0, f)e^{-t/\tau_p} = p_o \cos \omega t \cdot e^{-t/\tau_p}$ is the instantaneous over-pressure, and τ_p is the characteristic time constant associated with the exponential decay of the over-pressure amplitude with time.

Now, time-averaging over the rapid oscillations associated with $\cos \omega t = \cos 2\pi ft$, but **not** the slow-decay of the exponential, we have:

$$\langle p^2(t, f) \rangle = \langle p_o^2 \cos^2 \omega t \cdot e^{-2t/\tau_p} \rangle = p_o^2 \langle \cos^2 \omega t \rangle e^{-2t/\tau_p} = \frac{1}{2} p_o^2 e^{-2t/\tau_p}$$

Comparing this result with the above, we see that a relation exists between the two time constants τ_w and τ_p :

$$\tau_w = \tau_p/2 \quad \text{or:} \quad \tau_p = 2\tau_w$$

Hence, we obtain the following relations:

$$T_{60} = -\tau_w \ln(10^{-6.0}) = 13.8155 \tau_w = 13.8155 \cdot (\tau_p/2) = 6.90776 \tau_p$$

and:

$$T_{30} = -\tau_w \ln(10^{-3.0}) = 6.9078 \tau_w = 6.9078 \cdot (\tau_p/2) = 3.45388 \tau_p = \frac{1}{2} T_{60}$$

We have developed for the UIUC Physics 406 (and Physics 193) POM course a method which has enabled us to determine the over-pressure decay time constant τ_p to high accuracy by:

- a.) 24-bit digital recording the time-dependent signal output from a (reference) pressure mic situated somewhere in the large room, stimulated by either a single frequency, or white/pink noise emanating from a sound source located somewhere in the large room.
- b.) offline analyzing the pressure mic's time-dependent 24-bit digital signal data (*.wav format), using digital filtering techniques to window around the single frequency (in order to reject ambient noise), or use *e.g.* digital filters to window pink/white noise signals in 31 1/3-octave bands across the full audio spectrum, calculating the standard deviations $\sigma_p(t)$ of the over-pressure signals (which are linearly proportional to the over-pressure amplitudes) of the filtered signals in a short, running time window Δt (with $\tau_p (= 2\tau_w) \gg \Delta t \gg \tau = 1/f$), and then:
- c.) carrying out least-squares fits to decaying exponentials $\sigma_p(t) = \sigma_p^o e^{-t/\tau_p}$ associated with each of the windowed standard deviations, *e.g.* in the first 1/2 second (second 1/2 second) time interval – often there is more than one time constant, *e.g.* if the ceiling and floor of the large room are more absorptive than the walls of the room...

If interested, please see/read *e.g.* Serin Yoon's Fall 2012, Nathan Oliveira and Frank Horger's Fall 2010 and also Eric Egner's Fall 2007 UIUC 193 POM Final Reports, available on-line at the following URL:

http://courses.physics.illinois.edu/phys193/193_student_projects.html