## 2-D Interference-Diffraction with $N_y$ - $N_x$ Circular Apertures

In this example, we show plots of the sound intensity *vs*. angle and observer/listener position  $(x_{screen}, y_{screen})$  on a screen for the simplest theory of interference-diffraction pattern associated with a 2-D array of  $N_y$ - $N_x$  identical circular apertures, each of radius R, with transverse separation distances  $d_y$ ,  $d_x > R$ . This is an approximation to *e.g.* a 2-D array of  $N_y$ - $N_x$  loudspeakers mounted on an infinite baffle, as shown in the figure below. The observer/listener is located far from the apertures, a perpendicular distance L(m) away, such that the conditions  $R < d_y$ ,  $d_x \ll L$  and.  $\lambda \ll L$  both hold simultaneously, where  $\lambda(m)$  is the wavelength of the sound – this is the so-called "far-field" limit.



The expression for interference-diffraction associated with a 2-D array of  $N_y$ - $N_x$  identical circular apertures is given by the product of {independent} interference × diffraction factors:

$$I_{tot}(\theta) = I_o \underbrace{\left\{ \frac{\sin^2\left(N_x \delta_x(\theta_x)/2\right)}{\sin^2\left(\delta_x(\theta_x)/2\right)} \right\}}_{x-Interference} \cdot \underbrace{\left\{ \frac{\sin^2\left(N_y \delta_y(\theta_y)/2\right)}{\sin^2\left(\delta_y(\theta_y)/2\right)} \right\}}_{y-Interference} \cdot \underbrace{\left\{ \frac{2J_1(\rho(\theta))}{\rho(\theta)} \right\}^2}_{Diffraction}$$
  
and  $SIL(\theta) \equiv 10 \log_{10}\left(I_{tot}(\theta)/I_{ref}\right) (dB)$ 

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where  $I_o(Watts/m^2)$  is the maximum sound intensity associated with an individual circular aperture, the interference phases  $\delta_y(\theta_y) = k\Delta L_y(\theta_y) = kd_y \sin \theta_y$  and  $\delta_x(\theta_x) = k\Delta L_x(\theta_x) = kd_x \sin \theta_x (radians), \ k = 2\pi/\lambda (radians/m)$  is the wavenumber and  $\Delta L_y(\theta_y) = d_y \sin \theta_y (\Delta L_x(\theta_x) = d_x \sin \theta_x) (m)$  are the *y*-projected (*x*-projected) angle-dependent path length *differences*, respectively between pairs of adjacent sound sources in the *y*- (*x*-) direction to the observer/listener, located far away from the sound sources. The diffraction phase  $\rho(\theta) = kR \sin \theta = (2\pi/\lambda)R \sin \theta (radians)$  and  $J_1(\rho(\theta))$  is the ordinary Bessel function of the first kind, of order  $\nu = 1$ .  $I_{ref} \equiv 10^{-12} (Watts/m^2)$  is the reference sound intensity for the sound intensity level (SIL).

Interference <u>minima</u> – *i.e.* intensity zeroes (complete destructive interference) occur when the numerator factor  $N \, \delta/2 = \pm \pi, \pm 2\pi, \pm 3\pi, \ldots = n\pi, n = \pm 1, \pm 2, \pm 3, \ldots \underline{except}$  when the denominator factor simultaneously has  $\delta/2 = \pm \pi, \pm 2\pi, \pm 3\pi, \ldots = n\pi, n = \pm 1, \pm 2, \pm 3, \ldots$  then have <u>global maxima</u> of the intensity, where  $I_{\text{tot}} = N^2 I_0$ .

From simple trigonometry, it is easy to show that the path length difference  $\Delta L_y(\theta_y) = d_y \sin \theta_y$ , where  $\theta_y$  is the y-projected angle the observer/listener makes with respect to the normal, or forward axis of the array of  $N_y$  circular apertures, and similarly for  $\Delta L_x(\theta_x) = d_x \sin \theta_x$ .

Diffraction <u>minima</u> (intensity zeroes) occur at the non-trivial zeros of the Bessel function  $J_1(\rho)$ , which occur at  $\rho = 3.8317, 7.0156, 10.1735, 13.3237, 16.4706, 19.6159, ...$ 

The corresponding location of the observer's/listener's position  $y_{screen}$  on a screen located a perpendicular distance *L* away from the *N* sound sources is:  $r_{screen}(\theta) = L \tan \theta$ , or conversely:

$$\theta = \tan^{-1}(r_{screen}/L)$$
, where  $r_{screen} = \sqrt{x_{screen}^2 + y_{screen}^2}$  and  $\theta_y = \tan^{-1}(y_{screen}/L)$ ,  $\theta_x = \tan^{-1}(x_{screen}/L)$ .

We coded up the above formulas using MATLAB to make plots of  $I_{tot}$  vs.  $\theta$  and  $I_{tot}$  vs.  $(x_{screen}, y_{screen})$  e.g. for  $(N_y, N_x) = (1,1), (1,2), (2,1), (2,2), (2,4), (4,2), (4,4)$  for  $d_y = d_x = 1.0$  m and R = 1.0 m, with the following parameter values:  $I_o = 1 Watt/m^2$ , observer/listener distance (at  $\theta = 0$ ) of L = 10 m, the speed of propagation in free air/great-wide open:  $v_{air} = 343 m/s$  and frequency of f = 1000 Hz, thus  $\lambda = v_{air}/f = 0.345 m$ .

In the following figures, note that the angular width of the central maxima decreases as the radius of the circular aperture increases, since the diffraction phase  $\rho(\theta) = kR \sin \theta = (2\pi/\lambda)R \sin \theta$  (*radians*) is linearly proportional to *R*. Note also that the angular width of the central maxima decreases linearly with increasing frequency *f*, since the diffraction phase increases linearly with

$$\rho(\theta) = kR\sin\theta = (2\pi/\lambda)R\sin\theta = (2\pi f/v_{air})R\sin\theta (radians).$$

-2-

frequency:

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Note also that the angular width of the central maxima decreases as the number of circular apertures N increases. Note further that the number of maxima/minima increases linearly with increasing frequency f, since the y-, x-interference phase differences increase linearly with frequency:

$$\delta_{y}(\theta_{y}) = k\Delta L_{y}(\theta_{y}) = (2\pi/\lambda)\Delta L_{y}(\theta_{y}) = (2\pi f/v_{air})\Delta L_{y}(\theta_{y}) = (2\pi f/v_{air})d_{y}\sin\theta_{y}.$$
  
$$\delta_{x}(\theta_{x}) = k\Delta L_{x}(\theta_{x}) = (2\pi/\lambda)\Delta L_{x}(\theta_{x}) = (2\pi f/v_{air})\Delta L_{x}(\theta_{x}) = (2\pi f/v_{air})d_{x}\sin\theta_{x}.$$

Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (1, 1)$  with  $d_y = d_x = R = 1.0 m$ :





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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (1, 2)$  with  $d_y = d_x = R = 1.0 m$ :





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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (2, 1)$  with  $d_y = d_x = R = 1.0 m$ :





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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (2, 2)$  with  $d_y = d_x = R = 1.0 m$ :





theta-x (degrees)





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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (2, 4)$  with  $d_y = d_x = R = 1.0 m$ :



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270

theta-x (degrees)

330

300

210

240

Plots of  $I_{tot}$  vs.  $(x_{scr}, y_{scr})$  and SIL vs.  $(x_{scr}, y_{scr})$  for  $(N_y, N_x) = (2, 4)$  with  $d_y = d_x = R = 1.0 m$ :



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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (2, 4)$  with  $d_y = 3m, d_x = R = 1.0m$ :





theta-x (degrees)



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Plots of  $I_{tot}$  vs.  $(x_{scr}, y_{scr})$  and SIL vs.  $(x_{scr}, y_{scr})$  for  $(N_y, N_x) = (2, 4)$  with  $d_y = 3m, d_x = R = 1.0m$ :





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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (4, 2)$  with  $d_y = d_x = R = 1.0 m$ :



theta-x (degrees)

270

300

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240

Plots of  $I_{tot}$  vs.  $(x_{scr}, y_{scr})$  and SIL vs.  $(x_{scr}, y_{scr})$  for  $(N_y, N_x) = (4, 2)$  with  $d_y = d_x = R = 1.0 m$ :



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Polar plots of SIL vs.  $\theta_y$  and SIL vs.  $\theta_x$  for  $(N_y, N_x) = (4, 4)$  with  $d_y = d_x = R = 1.0 m$ :





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Plots of  $I_{tot}$  vs.  $(x_{scr}, y_{scr})$  and SIL vs.  $(x_{scr}, y_{scr})$  for  $(N_y, N_x) = (4, 4)$  with  $d_y = d_x = R = 1.0 m$ :



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Listing of the MATLAB code:

```
%______
% Intf_Diffn_2D_Circ_Aperture_Thy.m
% 2-D interference-diffraction associated with N circular apertures
% - simplest theory - far-field/plane-wave approx!
% Sound waves assumed to be propagating in free air/great wide-open!
% Ny circular apertures distributed symmetrically along horizontal y-axis
% Nx circular apertures distributed symmetrically along vertical x-axis
% We use a right-handed x-y-z coordinate system.
۶_____
% Written by Prof. Steven Errede Last Updated: Feb. 11, 2011 09:10 hr
ŝ
%______
close all;
clear all;
single
        thtxr(1800);
      thtxd(1800);
single
single thtyr(1800);
single thtyd(1800);
single Itotx1(1800);
single SILx1(1800);
single Itoty1(1800);
single SILy1(1800);
       xscr(2000);
single
single Itotx2(2000);
single SILx2(2000);
single yscr(2000);
single Itoty2(2000);
single SILy2(2000);
single Itotxy(2000,2000);
single LgItotxy(2000,2000);
single
       SILxy(2000,2000);
% Specify the # of y,x circular apertures:
Nyapr = 2; % 1; 2; 1; 2; 2; 4; 4; horizontal
Nxapr = 4; % 1; 1; 2; 2; 4; 2; 4; vertical
% Specify the numerical values of parameters:
Io = 1.0; % intensity from single slit (Watts/m^2)
      = 1.0*10^-12;% reference sound intensity (Watts/m^2)
Τr
Vair = 343.0; % speed of propagation of sound - free air (m/s)
freq = 1000.0; % frequency (Hz or cps)
lambda = Vair/freq; % wavelength (m)
Lobs = 10.0; % observer distance
Dx = 1.0; % x-distance between
                                           (m) n.b. lambda << Lobs
    = 1.0; % x-distance between apertures(m) n.b. Dx << Lobs
= 3.0; % y-distance between apertures(m) n.b. Dy << Lobs</pre>
Dy
Rapr = 1.0; % 0.6; 1.0; aperture radius (m) n.b. Rapr << Lobs
           1; % order of bessel function of 1st kind (see below)
     =
nu
% Calculate Itot, SIL vs. theta-y along horizontal y-axis @ x = 0:
8------
Thetad = -90.0; % angle theta of observer in degrees
dTheta = 0.1;
                 % step angle in degrees
for i = 1:1800;
    thtyd(i) = Thetad; % angle theta of observer in degrees
                                         -20-
```

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```
Thetar = (pi/180.0)*Thetad; % angle theta of observer in radians
    thtyr(i) = Thetar;
    deltay = ((2.0*pi*Dy)/lambda)*sin(Thetar); % int'f phase (radians)
          = ((2.0*pi*Rapr)/lambda)*sin(Thetar); % diffn phase (radians)
    rho
  Itoty1(i) = Io*(Nxapr)^2*(sin(Nyapr*deltay/2.0)/sin(deltay/2.0))^2
              *((2.0*bessel(nu,rho))/rho)^2;
   SILy1(i) = 10.0*log10(Itoty1(i)/Ir); % Sound Intensity Level (dB)
    Thetad = Thetad + dTheta; % increment angle for next calculation
end
<u>%______</u>
% Calculate Itot, SIL vs. yscreen along horizontal y-axis @ x = 0:
8_____
y = -50.00; % starting position on screen (m)
dy = 0.05; % step size on screen (m);
for i = 1:2000;
                 % position of observer on perp. screen (m)
    yscr(i) = y;
    Thetar = atan(y/Lobs); % angle theta of observer in radians
    deltay = ((2.0*pi*Dy)/lambda)*sin(Thetar); % int'f phase (radians)
    rho
          = ((2.0*pi*Rapr)/lambda)*sin(Thetar); % diffn phase (radians)
  Itoty2(i) = Io*(Nxapr)^2*(sin(Nyapr*deltay/2.0)/sin(deltay/2.0))^2
              *((2.0*bessel(nu,rho))/rho)^2;
   SILy2(i) = 10.0*log10(Itoty2(i)/Ir); % Sound Intensity Level (dB)
    y = y + dy; % increment screen position for next calculation
end
<u>%_____</u>
% Calculate 1-D Itot, SIL vs. theta-x along horizontal x-axis @ y = 0:
%_____
Thetad = -90.0; % angle theta of observer in degrees
dTheta = 0.1; % step angle in degrees
for i = 1:1800;
                             % angle theta of observer in degrees
    thtxd(i) = Thetad;
    Thetar = (pi/180.0)*Thetad; % angle theta of observer in radians
    thtxr(i) = Thetar;
    deltax = ((2.0*pi*Dx)/lambda)*sin(Thetar); % int'f phase (radians)
          = ((2.0*pi*Rapr)/lambda)*sin(Thetar); % diffn phase (radians)
    rho
  Itotx1(i) = Io*(Nyapr)^2*(sin(Nxapr*deltax/2.0)/sin(deltax/2.0))^2
              *((2.0*bessel(nu,rho))/rho)^2;
   SILx1(i) = 10.0*log10(Itotx1(i)/Ir); % Sound Intensity Level (dB)
    Thetad = Thetad + dTheta; % increment angle for next calculation
end
<u>%______</u>
\ Calculate 1-D Itot, SIL vs. xscreen along horizontal x-axis @ y = 0:
x = -50.00; % starting position on screen (m)
dx = 0.05; % step size on screen (m);
for i = 1:2000;
    xscr(i) = x;
                        % position of observer on perp. screen (m)
    Thetar = atan(x/Lobs); % angle theta of observer in radians
             ((2.0*pi*Dx)/lambda)*sin(Thetar); % int'f phase (radians)
    deltax =
           = ((2.0*pi*Rapr)/lambda)*sin(Thetar); % diffn phase (radians)
    rho
  Itotx2(i) = Io*(Nyapr)^2*(sin(Nxapr*deltax/2.0)/sin(deltax/2.0))^2
              *((2.0*bessel(nu,rho))/rho)^2;
   SILx2(i) = 10.0*log10(Itotx2(i)/Ir); % Sound Intensity Level (dB)
    x = x + dx; % increment screen position for next calculation
end
                                        -21-
```

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```
figure(01);
plot(thtyd,Itoty1,'b');
grid on;
xlabel('theta-y (degrees)');
ylabel('Intensity (Watts/m^{2})');
title('Intensity vs. theta-y at x = 0');
figure(02);
semilogy(thtyd,Itoty1,'b');
grid on;
xlabel('theta-y (degrees)');
ylabel('Intensity (Watts/m^{2})');
title('Log10 Intensity vs. theta-y at x = 0');
figure(03);
plot(thtyd,SILy1,'b');
grid on;
xlabel('theta-y (degrees)');
ylabel('SIL (dB)');
title('SIL vs. theta-y at x = 0');
figure(04);
polar(thtyr,SILy1,'b');
grid on;
xlabel('theta-y (degrees)');
ylabel('SIL (dB)');
title('Polar Plot of SIL vs. theta-y at x = 0');
figure(05);
plot(yscr,Itoty2,'b');
grid on;
xlabel('Yscreen (m)');
ylabel('Intensity (Watts/m^{2})');
title('Intensity vs. Yscreen at x = 0');
figure(06);
semilogy(yscr,Itoty2,'b');
grid on;
xlabel('Yscreen (m)');
ylabel('Intensity (Watts/m^{2})');
title('Log10 Intensity vs. Yscreen at x = 0');
figure(07);
plot(yscr,SILy2,'b');
grid on;
xlabel('Yscreen (m)');
ylabel('SIL (dB)');
title('SIL vs. Yscreen at x = 0');
figure(11);
plot(thtxd,Itotx1,'b');
grid on;
xlabel('theta-x (degrees)');
ylabel('Intensity (Watts/m^{2})');
title('Intensity vs. theta-x at y = 0');
figure(12);
semilogy(thtxd,Itotx1,'b');
grid on;
xlabel('theta-x (degrees)');
ylabel('Intensity (Watts/m^{2})');
title('Log10 Intensity vs. theta-x at y = 0');
figure(13);
plot(thtxd,SILx1,'b');
grid on;
xlabel('theta-x (degrees)');
ylabel('SIL (dB)');
title('SIL vs. theta-x at y = 0');
```

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```
figure(14);
polar(thtxr,SILx1,'b');
grid on;
xlabel('theta-x (degrees)');
ylabel('SIL (dB)');
title('Polar Plot of SIL vs. theta-x at y = 0');
figure(15);
plot(xscr,Itotx2,'b');
grid on;
xlabel('Xscreen (m)');
ylabel('Intensity (Watts/m^{2})');
title('Intensity vs. Xscreen at y = 0');
figure(16);
semilogy(xscr,Itotx2,'b');
grid on;
xlabel('Xscreen (m)');
ylabel('Intensity (Watts/m^{2})');
title('Log10 Intensity vs. Xscreen at y = 0');
figure(17);
plot(xscr,SILx2,'b');
grid on;
xlabel('Xscreen (m)');
ylabel('SIL (dB)');
title('SIL vs. Xscreen at y = 0');
۶_____
fprintf('\n Very CPU-intensive I(x,y) vs. x,y calcs - please be patient!! \n')
۶_____
8-----
% Calculate 2-D Itot, SIL vs. x,y-screen:
x = -50.00; % x-starting position on screen (m)
dx = 0.05; % x-step size on screen (m);
for j = 1:2000;
    xscr(j) = x; % x-position of observer on perp. screen (m)
    Thetax = atan(x/Lobs);
                             % x-projected angle theta-x in radians
    deltax = ((2.0*pi*Dx)/lambda)*sin(Thetax); % int'f phase (radians)
    y = -50.00; % y-starting position on screen (m)
   dy = 0.05; % y-step size on screen (m);
   for i = 1:2000;
        yscr(i) = y; % y-position of observer on perp. screen (m)
        rscr = sqrt((xscr(j))^2 + (yscr(i))^2); % radial pos'n on perp. screen (m)
        Thetar = atan(rscr/Lobs); % angle theta of observer in radians
        Thetay = atan(y/Lobs); % y-projected angle theta-y in radians
        deltay = ((2.0*pi*Dy)/lambda)*sin(Thetay); % int'f phase (radians)
               = ((2.0*pi*Rapr)/lambda)*sin(Thetar); % diffn phase (radians)
        rho
    Itotxy(j,i) = Io*(sin(Nxapr*deltax/2.0)/sin(deltax/2.0))^2
                   *(sin(Nyapr*deltay/2.0)/sin(deltay/2.0))^2
                   *((2.0*bessel(nu,rho))/rho)^2; % total intensity (Watts/m^2)
  LgItotxy(j,i) = log10(Itotxy(j,i)); % log10 of total intensity (Watts/m<sup>2</sup>)
     SILxy(j,i) = 10.0*log10(Itotxy(j,i)/Ir);
                                              % Sound Intensity Level (dB)
        v = v + dv;
                    % increment y-screen position for next calculation
   end
    x = x + dx; % increment x-screen position for next calculation
end
figure(21);
surf(xscr,yscr,Itotxy);
shading interp;
xlabel('Xscreen (m)');
ylabel('Yscreen (m)');
zlabel('Intensity (Watts/m^{2})');
title ('Intensity vs. Xscreen-Yscreen');
                                          -23-
```

```
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```

```
figure(22);
surf(xscr,yscr,LgItotxy);
shading interp;
xlabel('Xscreen (m)');
ylabel('Yscreen (m)');
zlabel('Log10(Intensity) (Watts/m<sup>4</sup>{2})');
title ('Log10(Intensity) vs. Xscreen-Yscreen');
figure(23);
surf(xscr,yscr,SILxy);
shading interp;
xlabel('Xscreen (m)');
ylabel('Yscreen (m)');
zlabel('SIL (dB)');
title ('SIL vs. Xscreen-Yscreen');
<u>%_____</u>
beep;
fprintf('\n Calculation of intf-diffn for 2-D array of Nx, Ny circular apertures completed !!!
\n')
8-----
```