

Lecture 24 - Cryogenics

Cooling usually involves a working substance (ex: gas, free e⁻ gas in a solid, He in ⁴He, etc.)

Two common principles for cooling are: using expansion of gas and evaporative cooling

Expansion engine

During isentropic expansion of a gas, we showed

$$pV^\gamma = \text{const.}$$

$$\gamma = \frac{5}{3} \quad \text{for ideal monatomic gas}$$

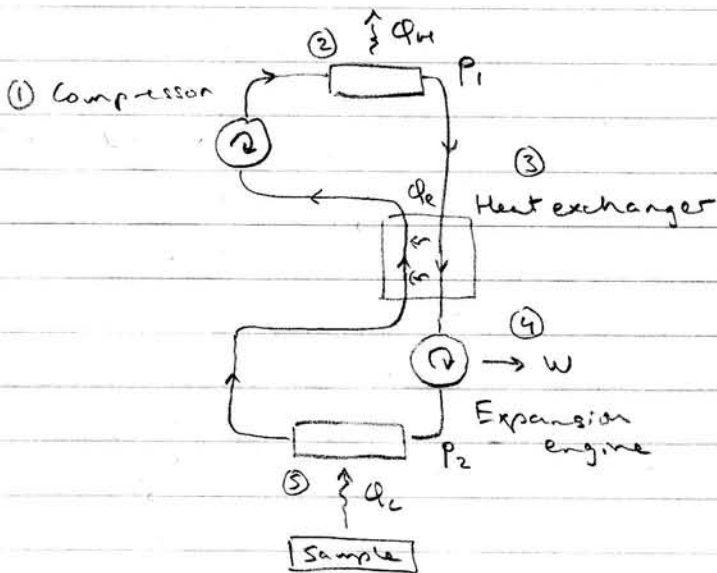
$$p T^{\gamma/(1-\gamma)} = \text{const.}$$

$$\text{since } pV = Nk_B T$$

$$\therefore \frac{T_2}{T_1} = \left(\frac{p_2}{p_1}\right)^{1-\gamma} = \left(\frac{p_2}{p_1}\right)^{2/5}$$

If gas is expanded $p_2 < p_1$ and $T_2 < T_1 \Rightarrow$ cooling

Usually expansion is done with a turbine, in a cycle:



- ① compression of gas
- ② Heat of compressed gas ejected into environment
- ③ Heat exchanged with cool return gas
- ④ Isentropic expansion of gas $\Rightarrow$ cooling
- ⑤ Cold gas extracts heat from sample

Expansion is isentropic, so no heat exchanged, but work is done by the gas:

$$W = (U_1 + p_1 V_1) - (U_2 + p_2 V_2) = H_1 - H_2$$

$U_1 + p_1 V_1$ = internal energy of incoming gas
+ work done by compressor

$U_2 + p_2 V_2$ = internal energy of outgoing gas
+ work to move gas against pressure p_2

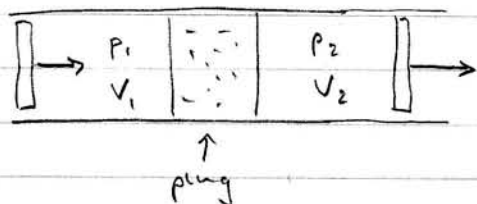
$$H = \frac{3}{2} N k_B T + N k_B T = \frac{5}{2} N k_B T \quad \text{for ideal, monatomic gas}$$

$$W = \frac{5}{2} N k_B (T_1 - T_2) \quad (T_1 > T_2)$$

This is an efficient way of cooling gas. However, can't be used to liquefy gases because of mechanical difficulties with turbine in expansion engine.

Throttling (or Joule-Thomson effect)

This method used to liquefy gases. Only requires porous plug or nozzle (i.e. no moving parts) to maintain pressure differential $p_1 > p_2$



Here, no net work is extracted by expanding gas

$$\therefore W = 0 = (U_1 + p_1 V_1) - (U_2 + p_2 V_2) = H_1 - H_2$$

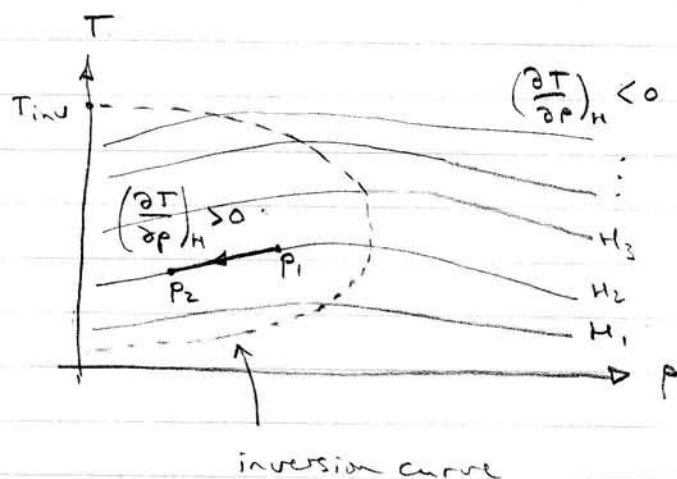
$\therefore H_1 = H_2$ constant enthalpy gas expansion

For an ideal gas $H = \frac{5}{2} N k_B T$ so constant H means constant $T \Rightarrow$ i.e. no cooling

However, for a real gas (i.e. van der Waals gas) H will depend on p, T - will get cooling as long as:

$$\left(\frac{\partial T}{\partial p} \right)_H > 0$$

Plot lines of constant H on p - T plane for van der Waals gas



Dotted line is the inversion curve, where sign of $(\frac{\partial T}{\partial p})_H$ switches

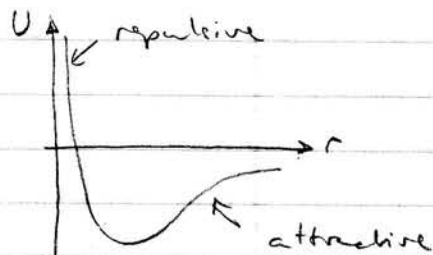
In region inside curve expansion will cool gas

Why do we need van der Waals model to explain this?

In ideal gas, U, H are independent of gas density n or pressure p

In van der Waals gas, there are long-range attractive forces (weak) and short-range repulsive forces (strong)

change in sign of $(\frac{\partial T}{\partial p})_H$ has to do with whether attractive or repulsive component dominates



$T > T_{inv}$ Kinetic energy of gas is so high, attractive forces are negligible but repulsive forces are not. Expansion = decrease in P.E. gas does $-W$ and T increases $\therefore \frac{\partial T}{\partial p} < 0$

$T < T_{inv}$ K.E. is low, attractive forces dominate.

Expansion = increase in P.E., gas does $+W$ and T decreases. $\therefore \frac{\partial T}{\partial p} > 0$

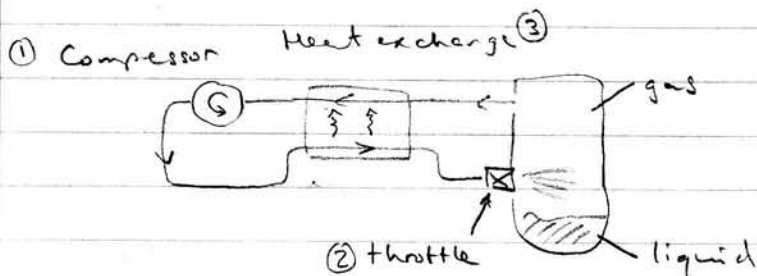
$$T_{inv}(N_2) = 621 \text{ K}$$

$$T_{inv}(H_2) = 205 \text{ K}$$

$$T_{inv}(^4\text{He}) = 5 \text{ K}$$

$\therefore$ To liquefy ^4He , first need to precool to $T < T_{inv}$. Can use liquid N_2 (77 K)

Liquefaction of gases commonly done in Linde cycle

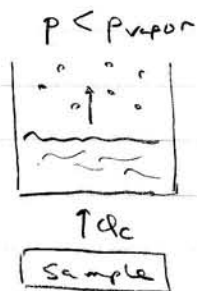


- ① Compressor pushes gas through throttling valve
- ② Gas cooled by throttling. Some is liquefied, vapor pumped back to compressor
- ③ Heat exchange between hot incoming gas and cool outgoing gas

Liquid $N_2 = 77K$ at $p = 1 \text{ atm}$
 $^4\text{He} = 4.2K$

Evaporative cooling

There is a latent heat with evaporation $L = T \Delta S$



If you pump away vapor above a liquid, so $p < \text{vapor pressure}$, then molecules leave liquid phase $\Rightarrow$ evaporation.

Requires latent heat L , supplied by Q_c from sample $\Rightarrow$ cooling

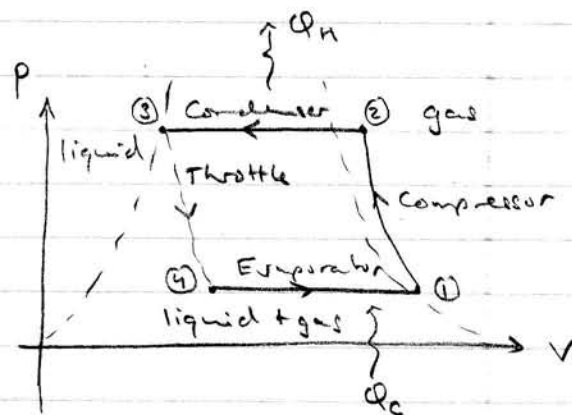
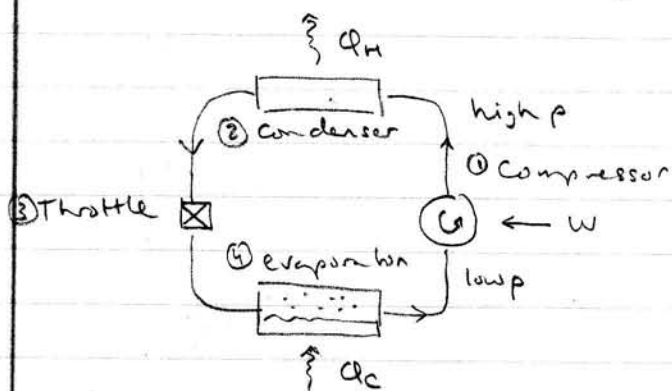
Generally $\frac{dQ_c}{dt} = L \frac{dN}{dt}$ $\frac{dN}{dt}$ = rate of removing molecules in vapor phase

As T decreases, so does p_{vapor} . (Recall $p_{\text{vapor}} = p_0 e^{-L/RT}$)
 so we need to pump harder to get $p < p_{\text{vapor}}$

For ^4He , practical limits to pumps take T from $4.2 \rightarrow 1.2K$

^3He is a lighter isotope of ^4He . Turns liquid at $3.2K$, has a higher vapor pressure, so it can be cooled further by evaporative cooling. Practically $3.2 \rightarrow 0.3K$

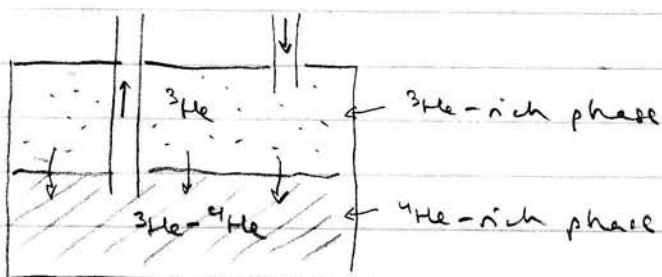
Modern refrigerators use throttling + evaporation to cool.
Working substance is Freon or hydrofluorocarbon
($T_{\text{boil}} = -29^\circ\text{C}$ and -47°C)



- ① Compression of gas raises T, p (isotropically)
- ② Hot gas expels heat Q_H to environment, condenses to high T, p liquid
- ③ Throttling cools liquid lowers pressure
- ④ Evaporation converts liquid to gas, extracts Q_C from cold reservoir (i.e. refrigerator or freezer)

Dilution refrigerator

Preferred method for cooling below $\sim 0.3\text{K}$ since 1960's
Uses mixture of ^4He , ^3He . Below 0.87K , ^4He and ^3He are immiscible $\Rightarrow$ mixture phase separates into a ^3He -rich phase (essentially pure ^3He) and a ^4He -rich phase (has 6% ^3He). ^3He -rich phase is lighter $\Rightarrow$ floats on top



^4He is essentially inert
 ^3He is a fermion gas

Principle of cooling is similar to evaporation

As ^3He molecules move from top ^3He -rich phase to bottom ^4He -rich phase, they are diluted and gain entropy $\Delta S = S(^4\text{He-rich}) - S(^3\text{He-rich})$

This is like a latent heat $L = C_p = T\Delta S$ extracted from cooling sample

^3He in ^4He -rich phase acts like vapor, ^3He -rich phase as liquid.

To get constant rate of cooling, need to dilute ^3He in ^4He -rich phase below 6%, then ^3He will evaporate into ^4He

Dilution cooling works from $\sim 0.5\text{K} \rightarrow 10\text{mK}$

Isentropic demagnetization

This relies on paramagnetic properties of working substance
Consider N spins (electronic or nuclear) in a B-field

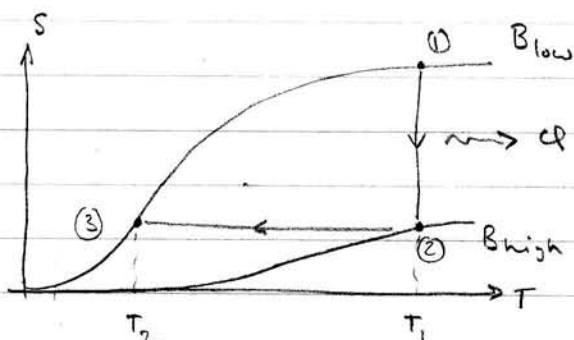
$$Z_1 = e^{\mu B/k_B T} + e^{-\mu B/k_B T} = 2 \cosh \frac{\mu B}{k_B T}$$

Showed in homework

$$S = N k_B \left[\ln \left(2 \cosh \frac{\mu B}{k_B T} \right) - \frac{\mu B}{k_B T} \tanh \frac{\mu B}{k_B T} \right]$$

Notice S is a function of $\frac{B}{T}$: $S\left(\frac{B}{T}\right)$

Plot S for 2 B-fields B_{high} , B_{low}



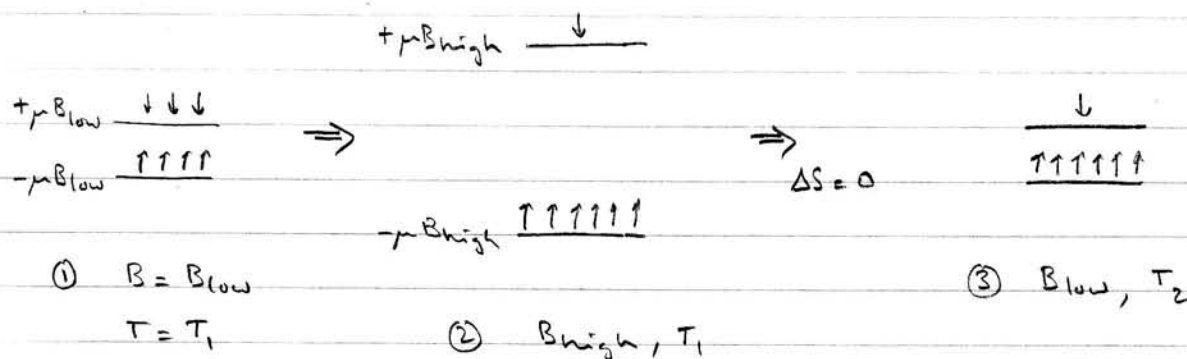
① → ② Increase B ($B_{low} \rightarrow B_{high}$) isothermally. Spins become more ordered, S decreases (Q out)

② → ③ Decrease B isothermally system cools from $T_1 \rightarrow T_2$

Since $S = S\left(\frac{B}{T}\right)$ $\frac{B_{high}}{T_1} = \frac{B_{low}}{T_2}$

$\therefore T_2 = T_1 \frac{B_{low}}{B_{high}} \ll T_1$

Energy level diagram



During second step, relative populations are maintained ($\Delta S = 0$)
 $\therefore T$ decreases

With this approach can get to 1mK for electronic paramagnets
1μK for nuclear paramagnets!

Why is there a limit? If you make $B_{low} = 0$, shouldn't $T_2 = 0$?
No! Interactions between spins are important below a certain T
Get ferromagnetic ordering. As we saw for Weiss model, interactions are like residual B-field $\therefore B_{low} \geq 0$ practically