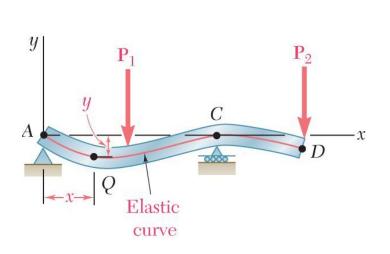
Chapter 12: Deflection of Beams and Shafts

Chapter Objectives

- ✓ Determine the deflection and slope at specific points on beams and shafts, using various analytical methods including:
 - The integration method
 - The method of superposition

Deflection of beams

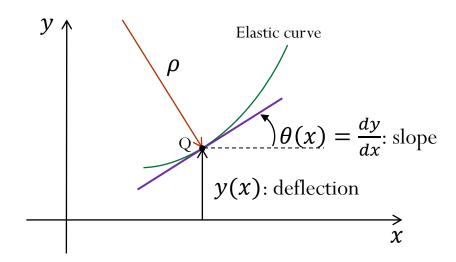
• <u>Goal</u>: Determine the deflection and slope at specified points of beams and shafts





- Solve statically indeterminate beams: where the number of reactions at the supports exceeds the number of equilibrium equations available.
- Maximum deflection of the beam: Design specifications of a beam will generally include a maximum allowable value for its deflection

Moment-Curvature equation:



$$\frac{d^2y}{dx^2} = \frac{M(x)}{EI}$$

 $\frac{d^2y}{dx^2} = \frac{M(x)}{EI}$ Governing equation of the elastic curve

- Elastic curve equation for constant E and I: E I y'' = M(x)
- Differentiating both sides gives: $E I y''' = \frac{dM(x)}{dx} = V(x)$
- Differentiating again: $E I y'''' = \frac{dV(x)}{dx} = -w(x)$
- In summary, we have:

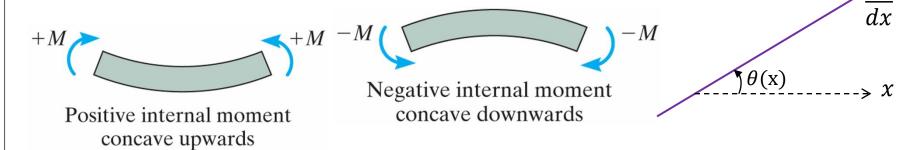
$$y(x)$$
: deflection

y'(x): slope E I y''(x): bending moment

E I y'''(x): shear force

E I y''''(x): distributed load

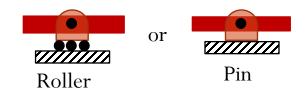
• Sign conventions:

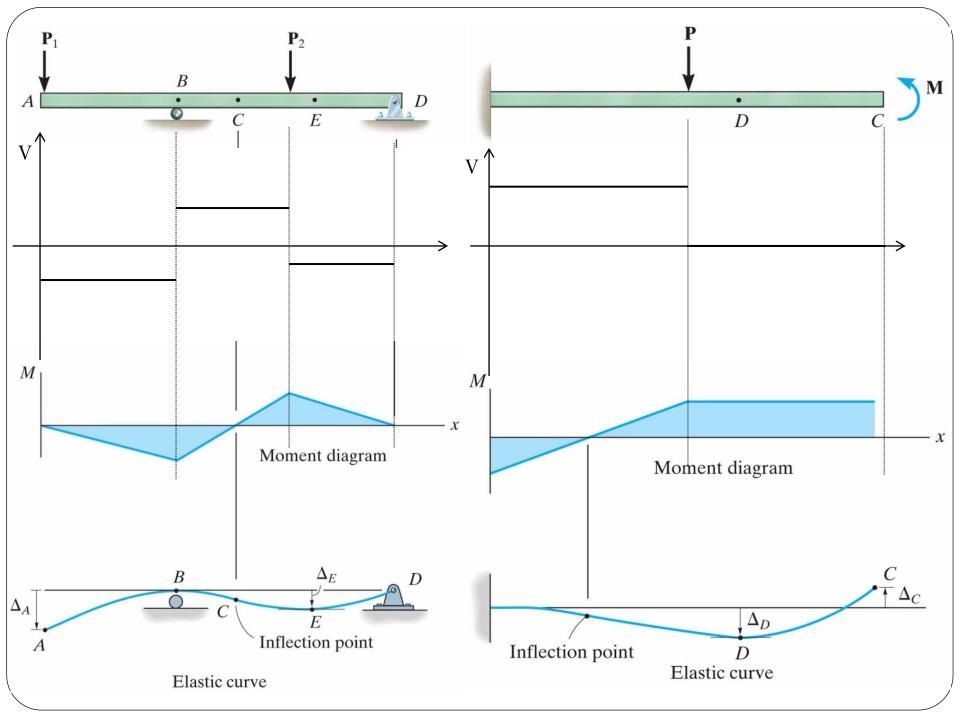


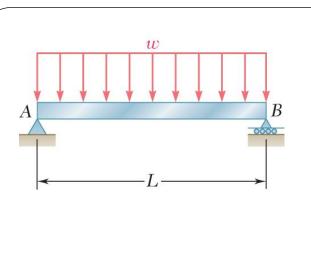
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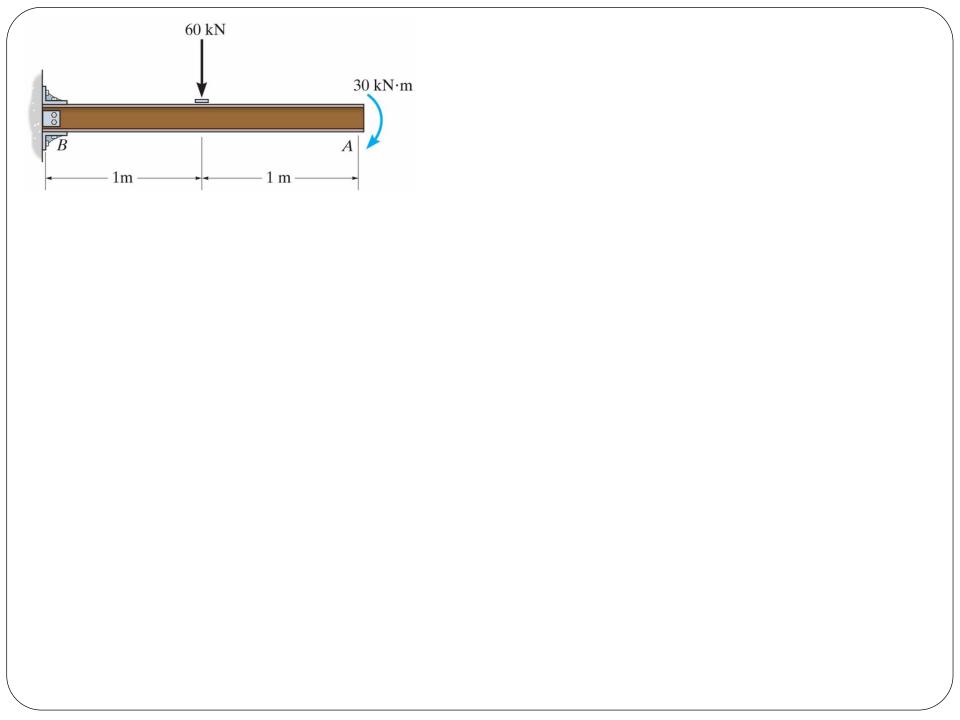
• Boundary conditions











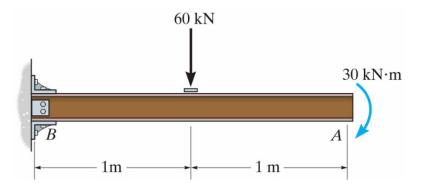
Superposition principle

Many common beam deflection solutions have been worked out – see your formula sheet!

If we'd like to find the solution for a loading situation that is not given in the table, we can use superposition to get the answer: represent the load of interest as a combination of two or more loads that are given in the table, and the resulting deflection curve for this loading is simply the sum of each curve from each loading treated separately

| Beam Deflection | | | | | | |
|---|------------------------|-------------------------|---|--|--|--|
| Diagram | Max. Deflection | Slope at End | Elastic Curve | | | |
| Diagram | y_{max} | θ | y(x) | | | |
| y p x y | $-\frac{PL^3}{3EI}$ | $-\frac{PL^2}{2EI}$ | $y(x) = \frac{P}{6EI} \left(x^3 - 3Lx^2 \right)$ | | | |
| y w x y | $-\frac{wL^4}{8EI}$ | $-\frac{wL^3}{6EI}$ | $y(x) = -\frac{w}{24EI} \left(x^4 - 4Lx^3 + 6L^2x^2 \right)$ | | | |
| y x y | $-\frac{ML^2}{2EI}$ | $-rac{ML}{EI}$ | $y(x) = -\frac{M}{2EI}x^2$ | | | |
| $\begin{vmatrix} y \\ y \\ y \\ -L \end{vmatrix} x$ | $-\frac{5wL^4}{384EI}$ | $\pm \frac{wL^3}{24EI}$ | $y(x) = -\frac{w}{24EI} \left(x^4 - 2Lx^3 + L^3x \right)$ | | | |
| y L P L Z Y | $-\frac{PL^3}{48EI}$ | $\pm \frac{PL^2}{16EI}$ | For $0 \le x \le \frac{L}{2}$ $y(x) = \frac{P}{48EI} \left(4x^3 - 3L^2x\right)$ | | | |

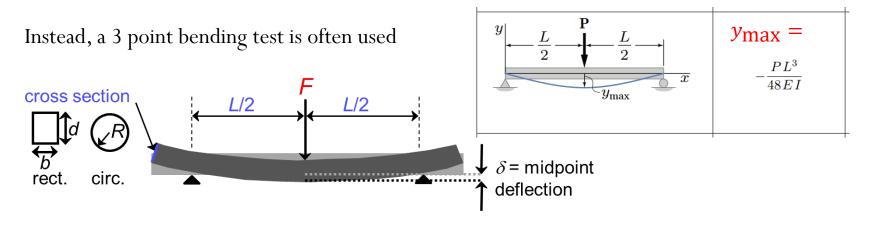
Obtain the deflection at point A using the superposition method – compare with the result obtained using the integration method!



| Diagram | Max. Deflection | Slope at End | Elastic Curve |
|---|---------------------|---------------------|---|
| 2 111911111 | y_{max} | θ | y(x) |
| y P y | $-\frac{PL^3}{3EI}$ | $-\frac{PL^2}{2EI}$ | $y(x) = \frac{P}{6EI} \left(x^3 - 3Lx^2 \right)$ |
| y x y | $-\frac{ML^2}{2EI}$ | $-\frac{ML}{EI}$ | $y(x) = -\frac{M}{2EI}x^2$ |

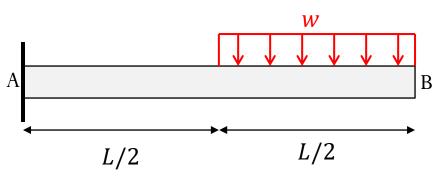
Practical application: measure stiffness of brittle material

It can be difficult to perform a tension test on brittle materials — can easily crack at grips and can only withstand small amount of strain



Find an expression for the stiffness E of the material, given the geometry, applied load F, and deflection δ at the midpoint

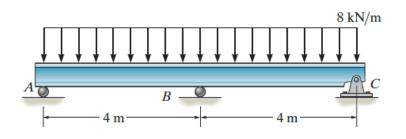
Assuming failure occurs at a force F_f , find an expression for the stress at failure σ_f

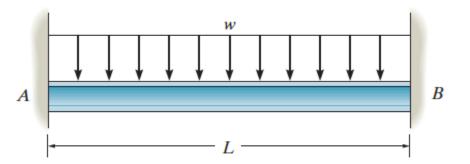


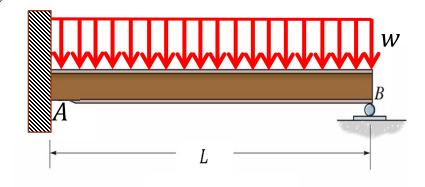
Find the deflection at point B at the end of the cantilever beam

| Beam Deflection | | | | | |
|-----------------|---------------------|---------------------|---|--|--|
| Diagram | Max. Deflection | Slope at End | Elastic Curve | | |
| Diagram | y_{max} | θ | y(x) | | |
| y_{\max} | $-\frac{wL^4}{8EI}$ | $-\frac{wL^3}{6EI}$ | $y(x) = -\frac{w}{24EI} \left(x^4 - 4Lx^3 + 6L^2x^2 \right)$ | | |

Indeterminate problems

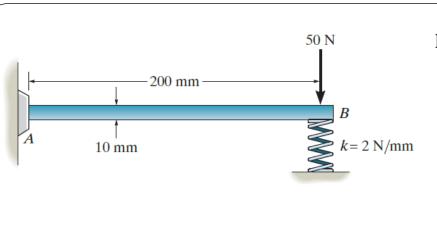




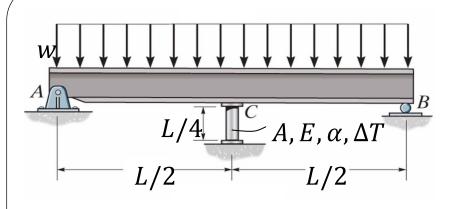


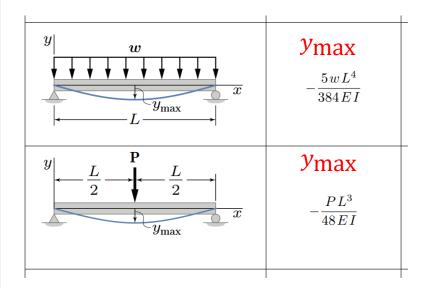
Obtain the reaction at the support B using

- Integration method Superposition method



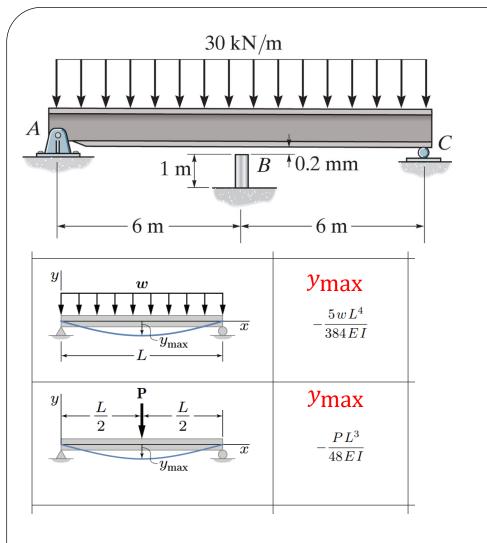
Determine the deflection at B



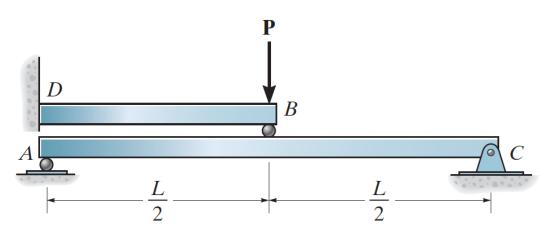


The beam is supported by a pin at A, a roller at B, and a deformable post at C. The post has length L/4, cross-sectional area A, modulus of elasticity E, and thermal expansion coefficient α . The beam has constant moment of inertia $I = A L^2$ and modulus of elasticity E (the same as the post).

(a) Determine the internal force in the post when the distributed load w is applied AND the post experiences an increase in temperature ΔT , where $\Delta T > 0$.



Before the uniform distributed load is applied on the beam, there is a small gap of 0.2 mm between the beam and the post at B. Determine the support reactions at A, B, and C. The post at B has a diameter of 40 mm, and the moment of inertia of the beam is $I = 875 \times 10^6 \text{ mm}^4$. The post and the beam are made of material having a modulus of elasticity of E = 200 GPa.



| Diagram | Max. Deflection | |
|--|----------------------|--|
| g | y_{max} | |
| y p x y | $-rac{PL^3}{3EI}$ | |
| $y \longrightarrow \frac{L}{2} \longrightarrow \frac{P}{2} \longrightarrow \frac{L}{2} \longrightarrow x$ $y \longrightarrow y_{\text{max}}$ | $-\frac{PL^3}{48EI}$ | |

Find the reaction force at point C using superposition methods